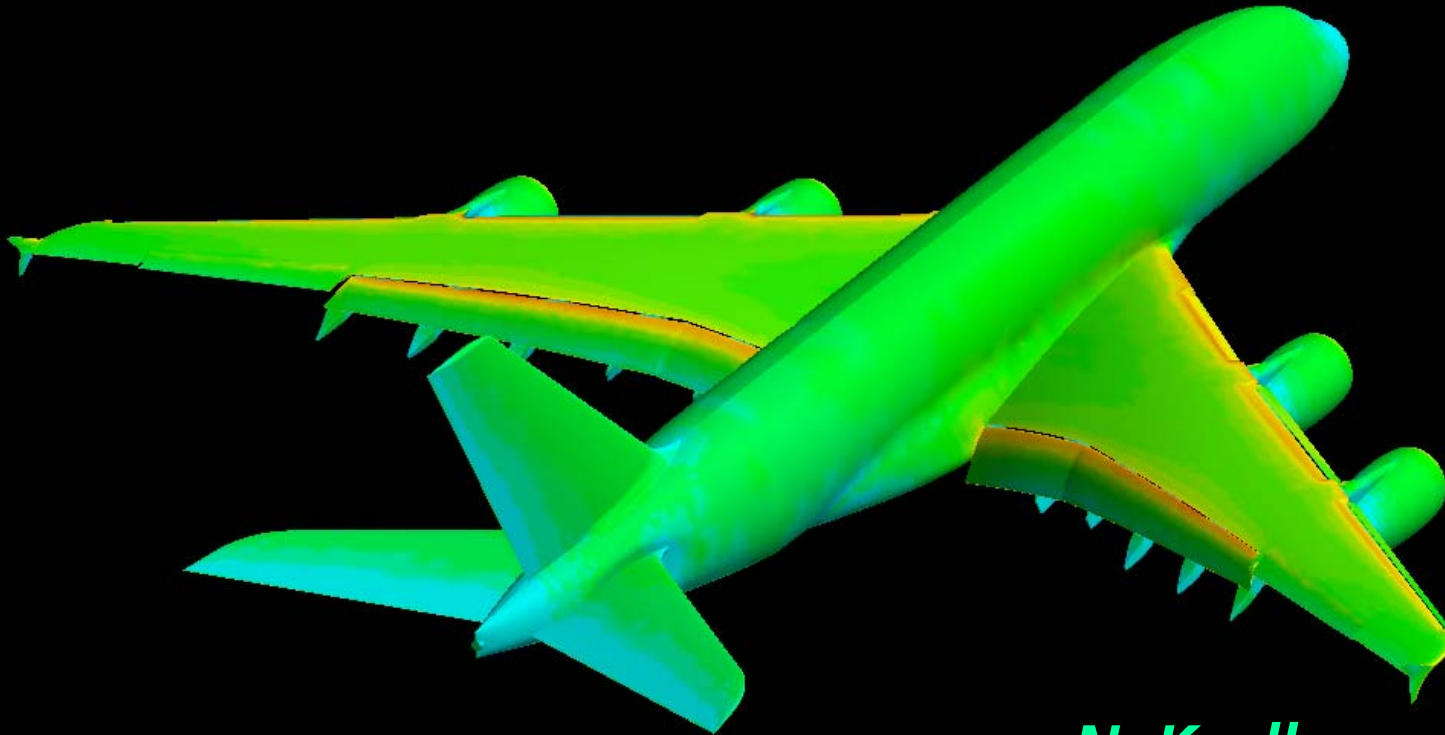




# Flow Simulation and Shape Optimization for Aircraft Design

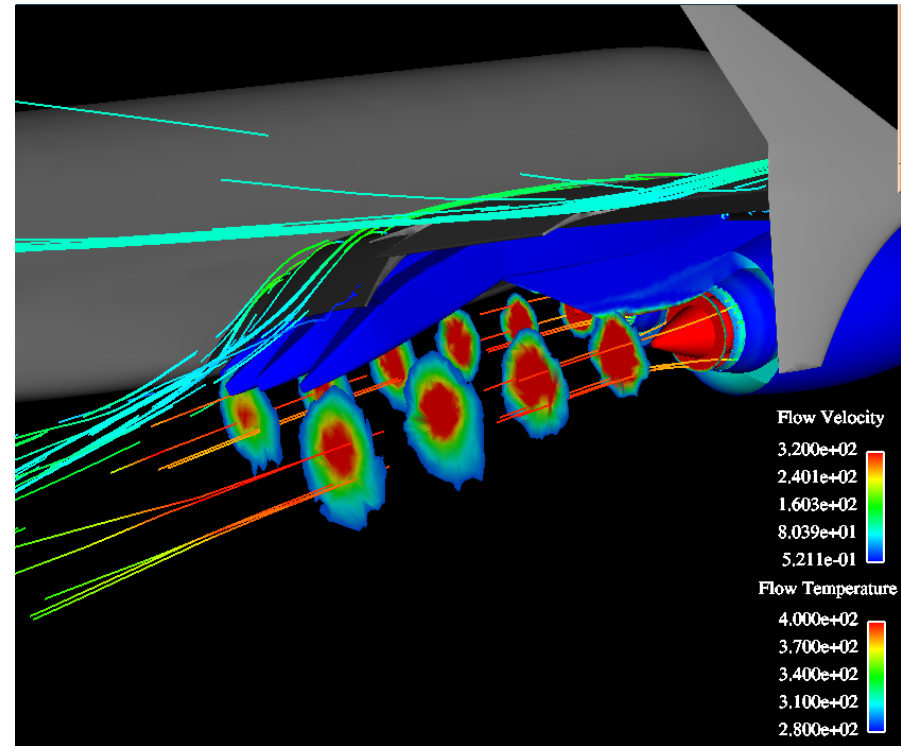


*N. Kroll*

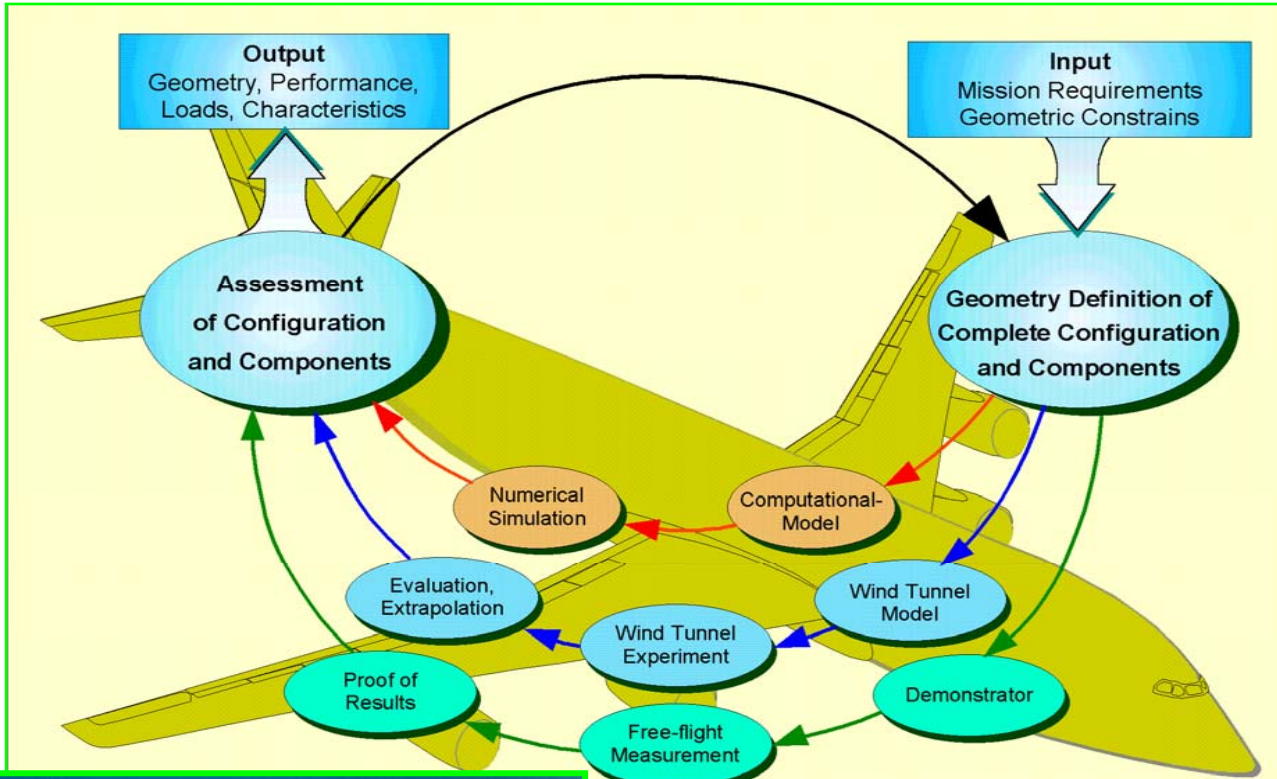
DLR (German Aerospace Center)  
Institute of Aerodynamics and Flow Technology  
Braunschweig

## Outline

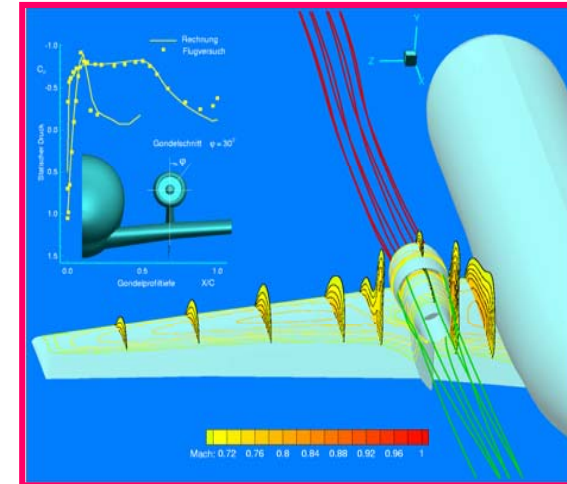
- Introduction
- Flow Solvers
- Validation & Applications
- Shape Design and Optimization
- Perspectives



# Aerodynamic Design Cycle



## Computational Fluid Dynamics (CFD)



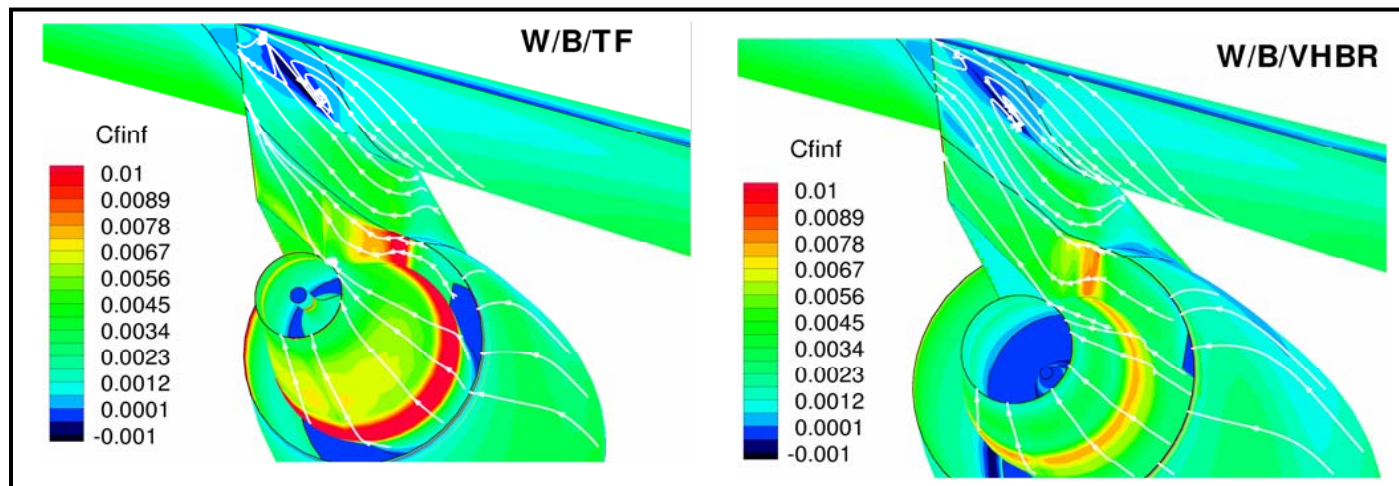
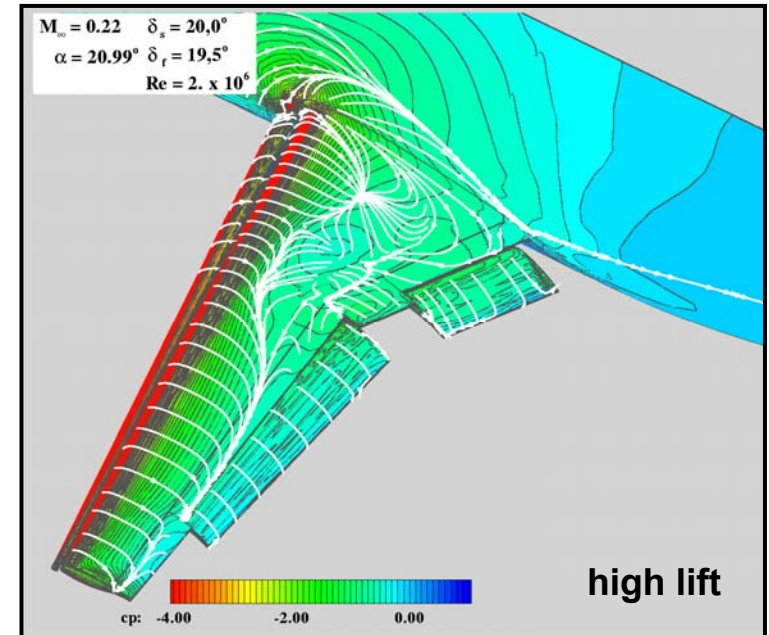
flight test



wind tunnel experiment

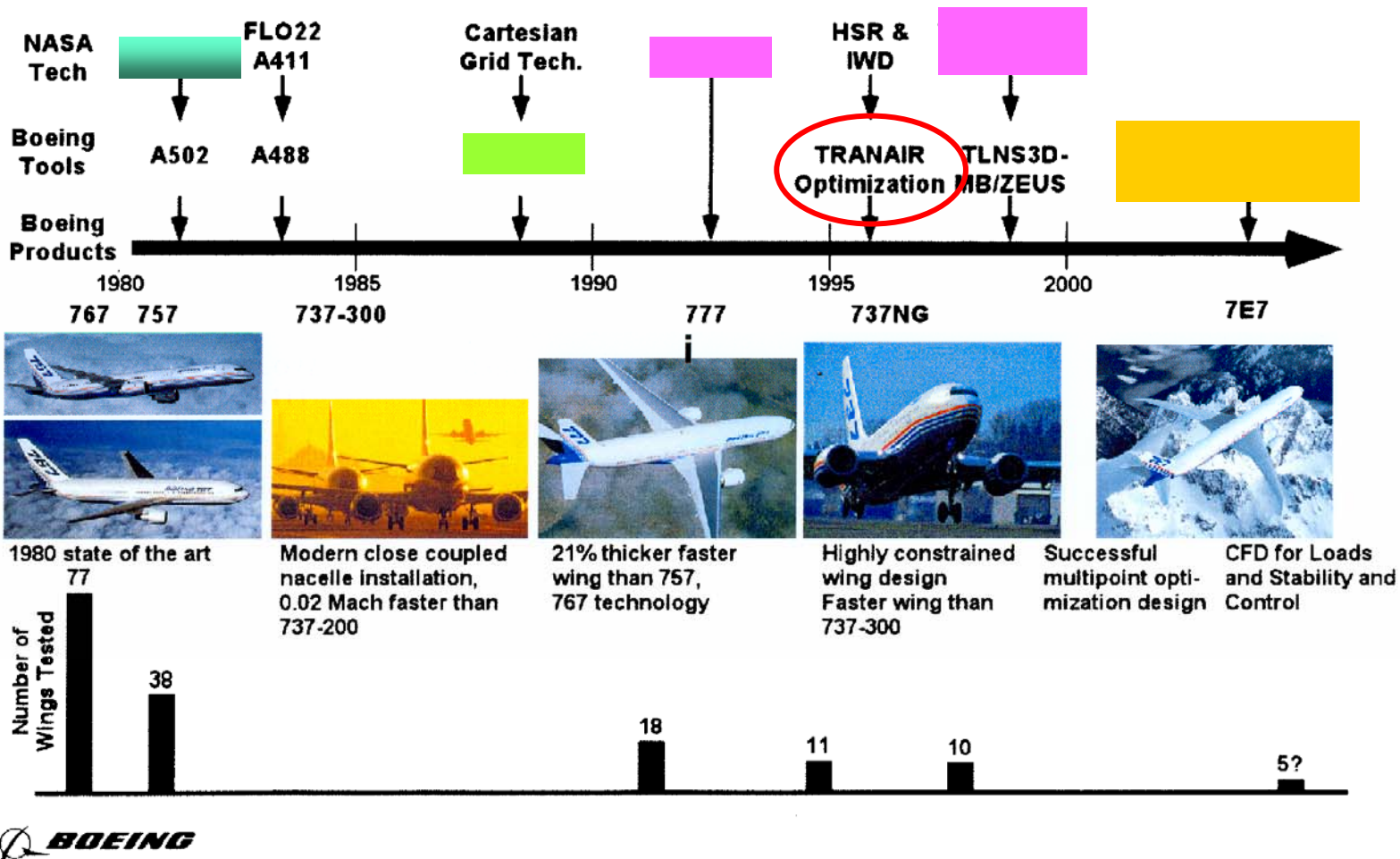
## Objectives of CFD

- detailed analysis of complex flow fields
- cost efficient configuration studies
- extrapolation of wind tunnel results to free flight conditions
- shape optimization





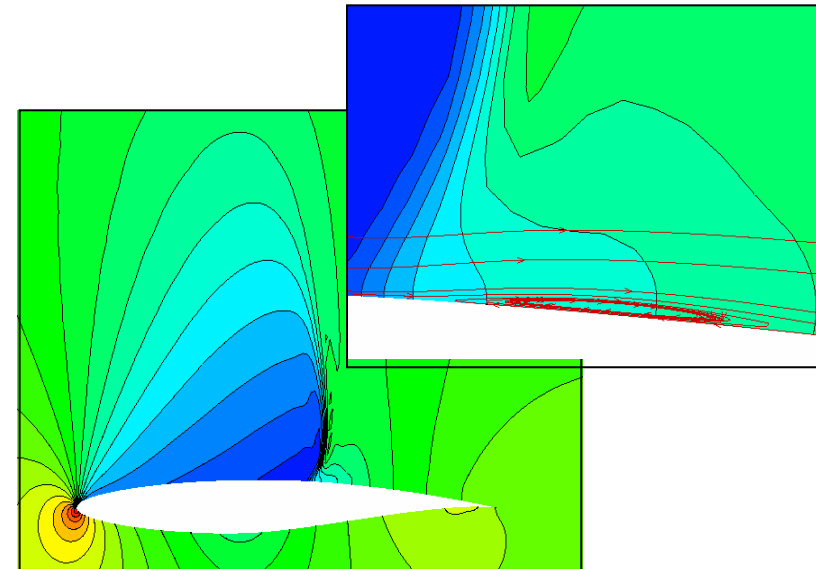
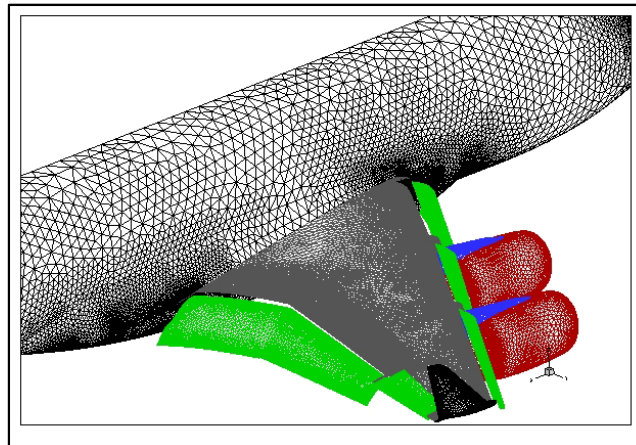
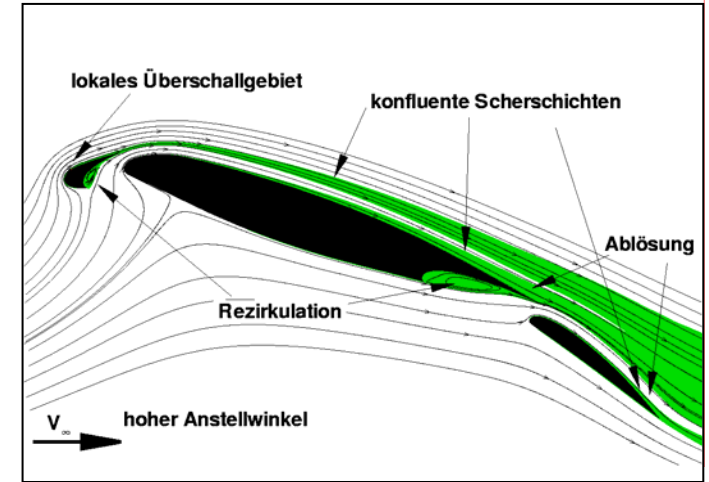
# Impact of CFD on Wind Tunnel Testing



## Effect of CFD on Configuration Lines Wind Tunnel Development Testing

## Requirements on CFD

- high level of physical modeling
  - compressible flow
  - transonic flow
  - laminar - turbulent flow
  - high Reynolds numbers (60 million)
  - large flow regions with flow separation
  - steady / unsteady flows
- complex geometries
- short turn around time





# Use of CFD in Aerodynamic Aircraft Design

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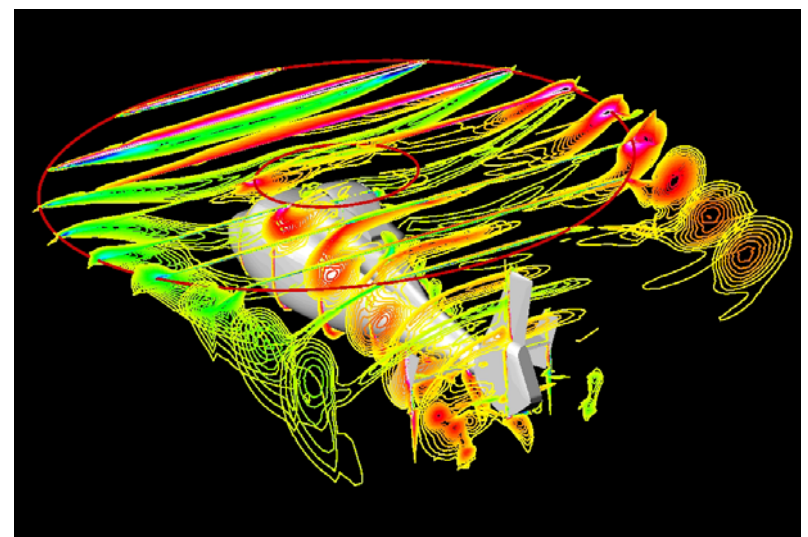
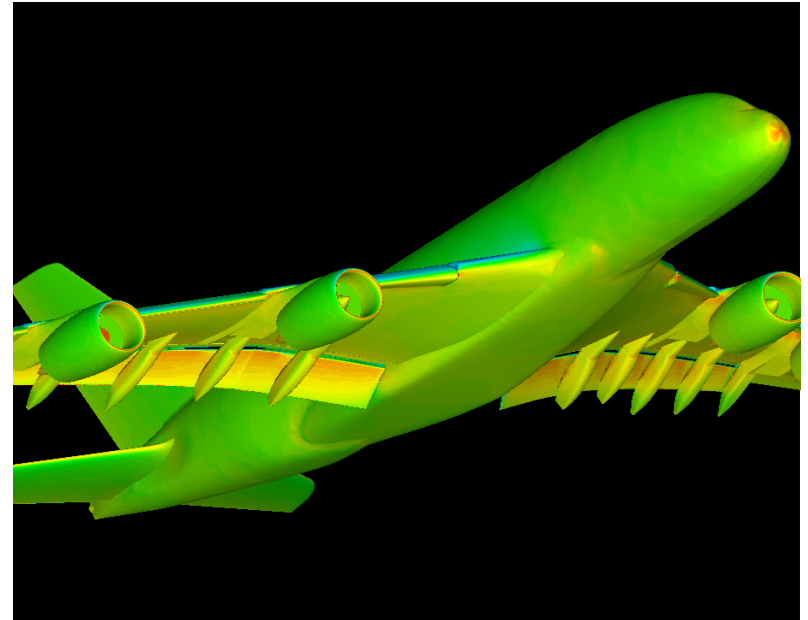
## Consequences

- solution of 3D compressible Reynolds averaged Navier-Stokes equations
- turbulence models based on transport equations (2 – 6 eqn)
- models for predicting laminar-turbulent transition
- flexible grid generation techniques with high level of automation (block structured grids, overset grids, unstructured/hybrid grids)
- link to CAD-systems
- efficient algorithms (multigrid, grid adaptation, parallel algorithms...)
- large scale computations ( ~ 10 - 25 million grid points)

## Main Goal

Development/validation of a **national CFD software** for complete aircraft applications which

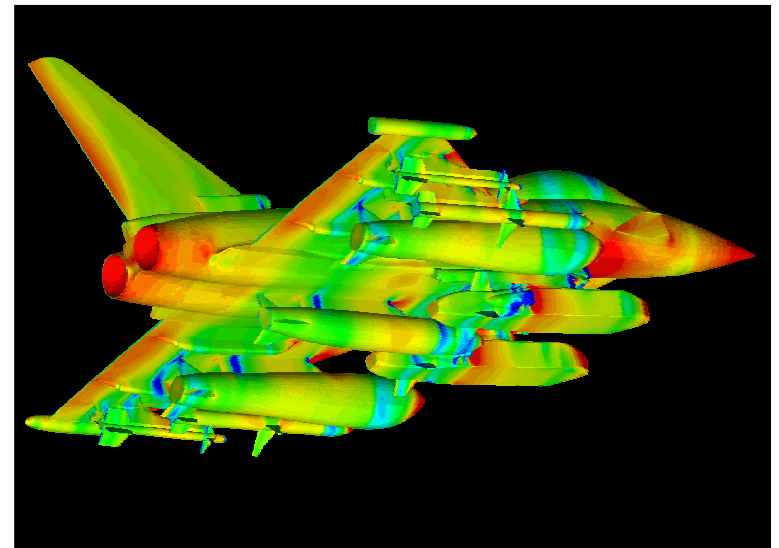
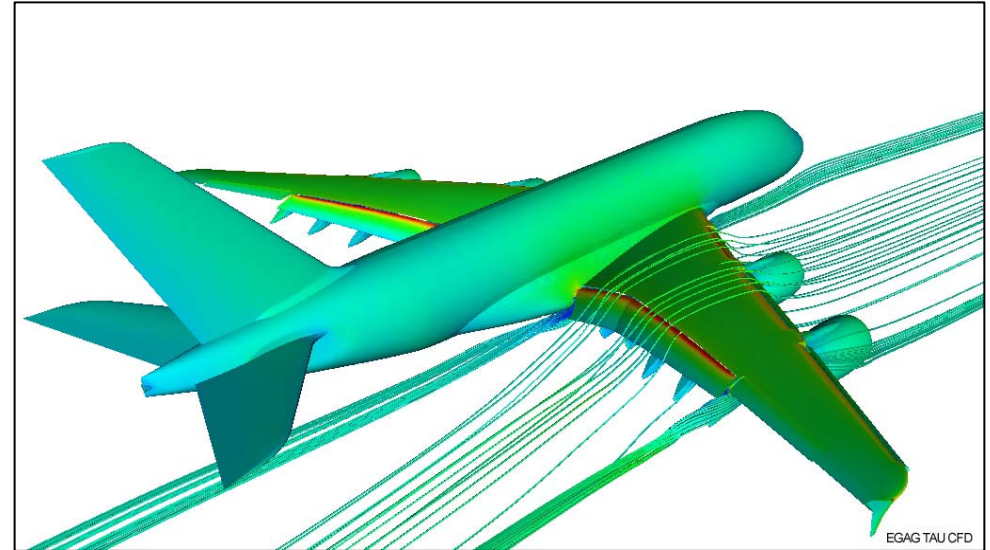
- allows Navier-Stokes computations for 3D complex configurations at cruise and high-lift conditions
- establishes numerical flow simulation as a routinely used tool at DLR and in German aircraft industry
- CFD kernel for multidisciplinary simulation and optimization
- serves as a development platform for universities

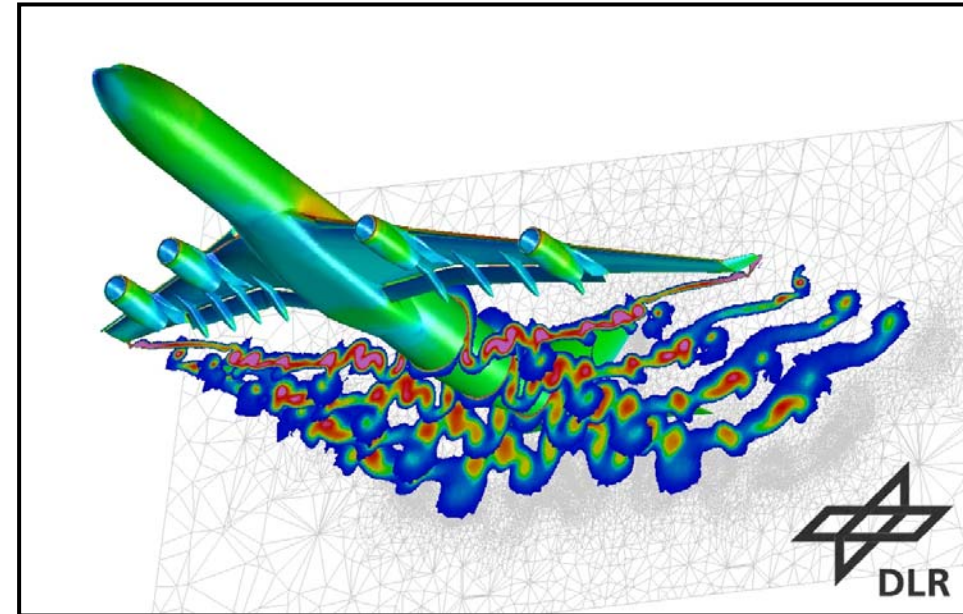
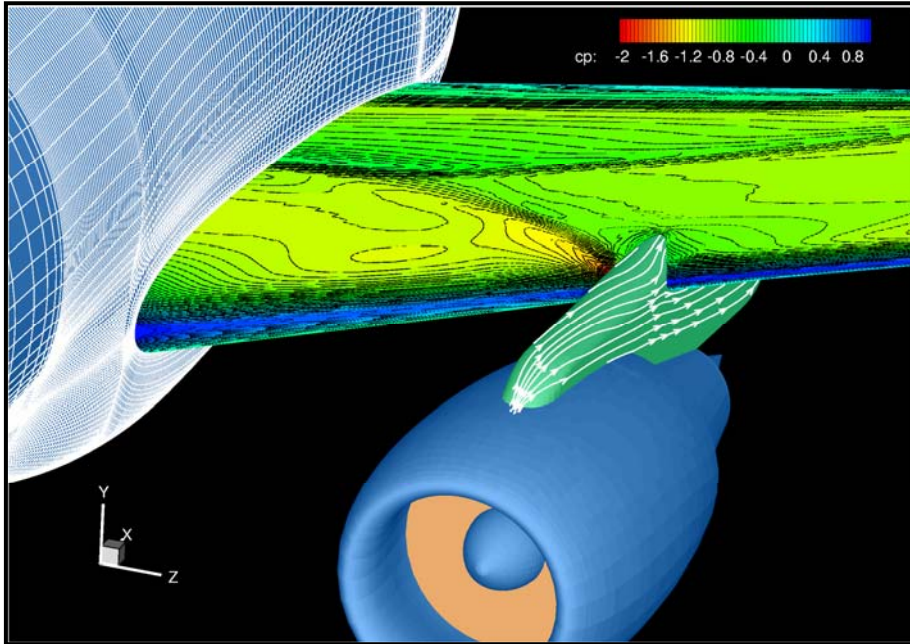




## Approach

- common effort of aircraft industry, DLR, several universities
- development activities driven by industrial requirements
- **single software platform for research and industrial application**
- early implementation of software components in industry
- validation based on industrial relevant applications
- links to other disciplines for multidisciplinary simulations
- quality assurance of software system
- open source policy
- **coordination and software support by DLR**





## Structured RANS solver **FLOWer**

- block-structured grids
- moderate complex configurations
- fast algorithms (unsteady flows)
- design option

## Unstructured RANS solver **TAU**

- hybrid grids
- very complex configurations
- grid adaptation
- fully parallel software

## Physical model

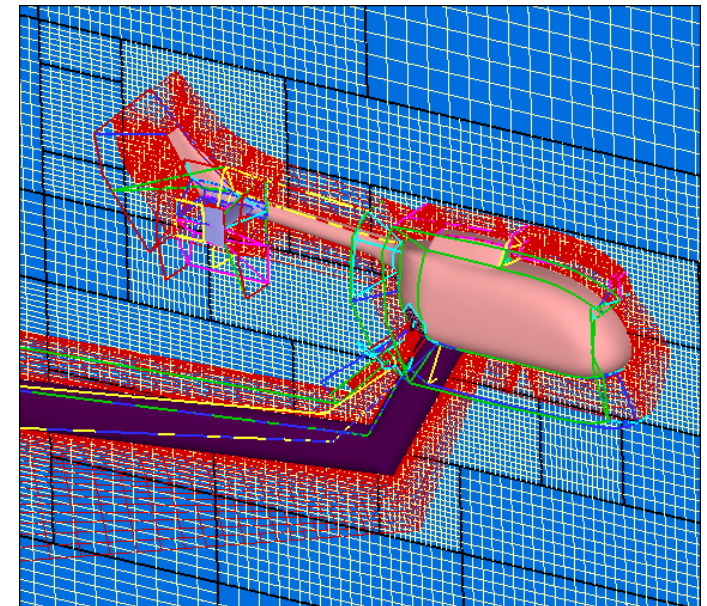
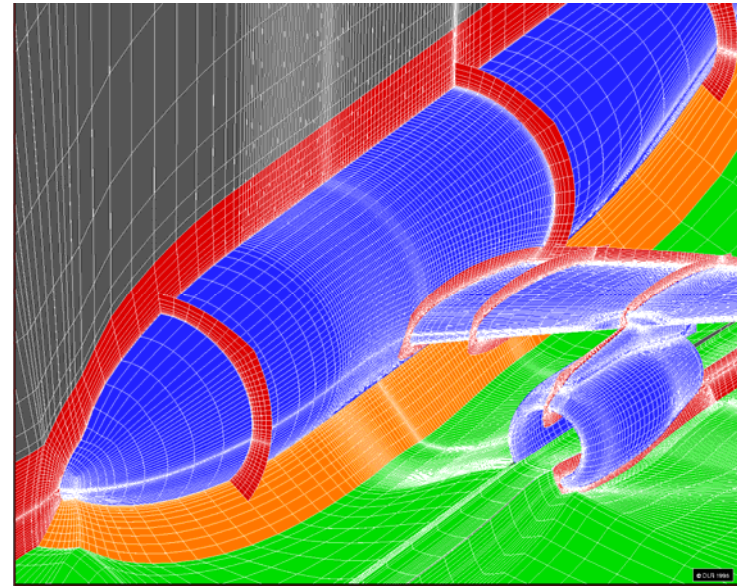
- 3D compressible Navier-Stokes equations
- arbitrarily moving bodies
- steady and time accurate flows
- state-of-the-art turbulence models (RSM)

## Grid strategy

- block-structured grids
- discontinuous block boundaries
- overset grids (Chimera)
- deforming grids

## Numerical algorithms

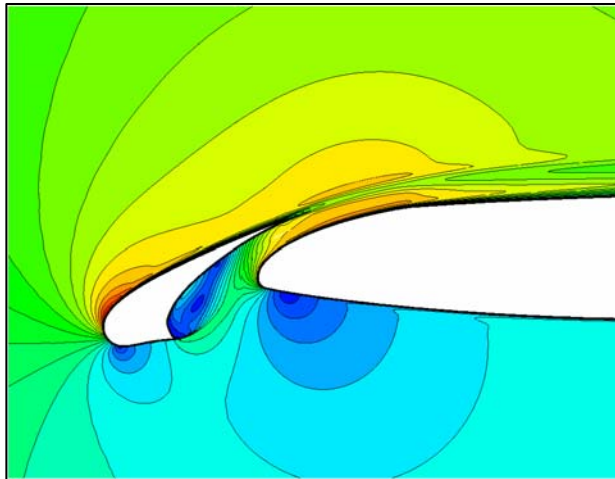
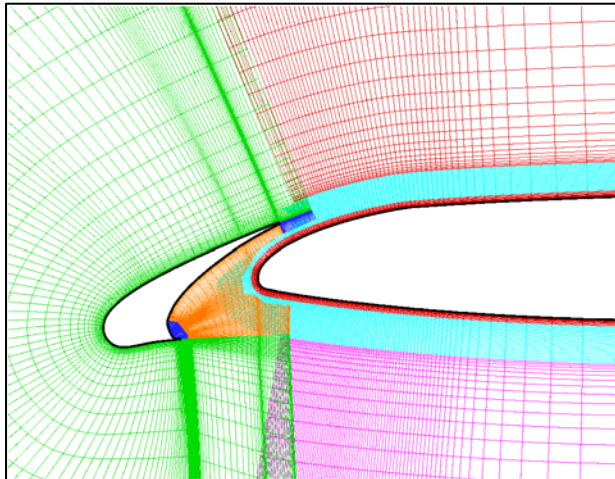
- 2nd order finite volume discretization (cell centered & cell vertex option)
- central and upwind schemes
- multigrid
- implicit treatment of turbulence equations
- implicit schemes for time accurate flows
- preconditioning for low speed flow
- vectorization & parallelization
- adjoint solver



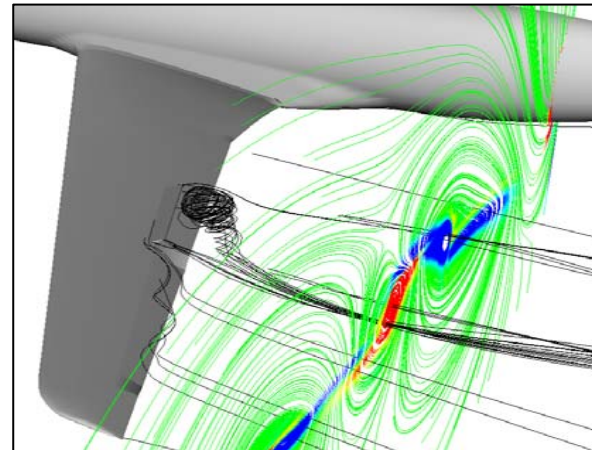
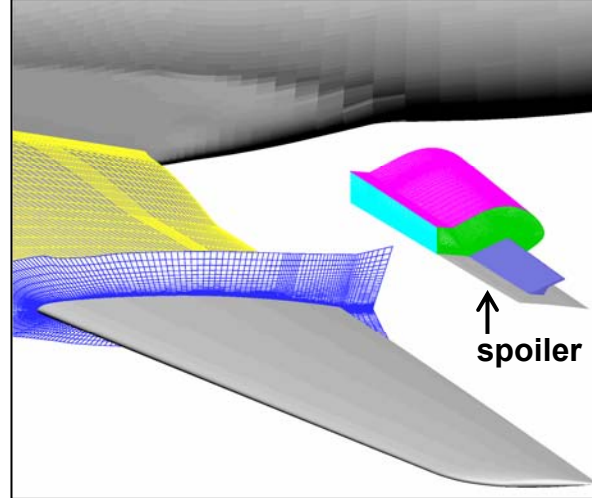


# FLOWer - Overset Grids (Chimera)

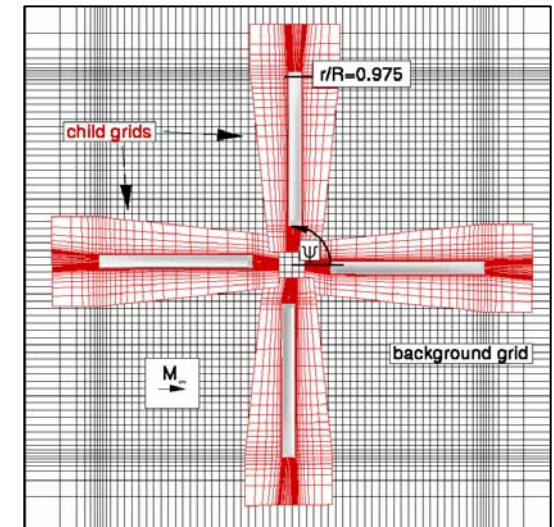
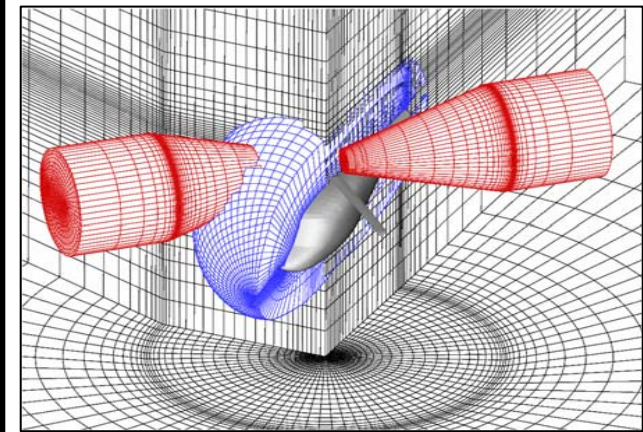
*simplification of grid generation*



*increased flexibility in application*



*efficient treatment of bodies in relative motion*





## Physical model

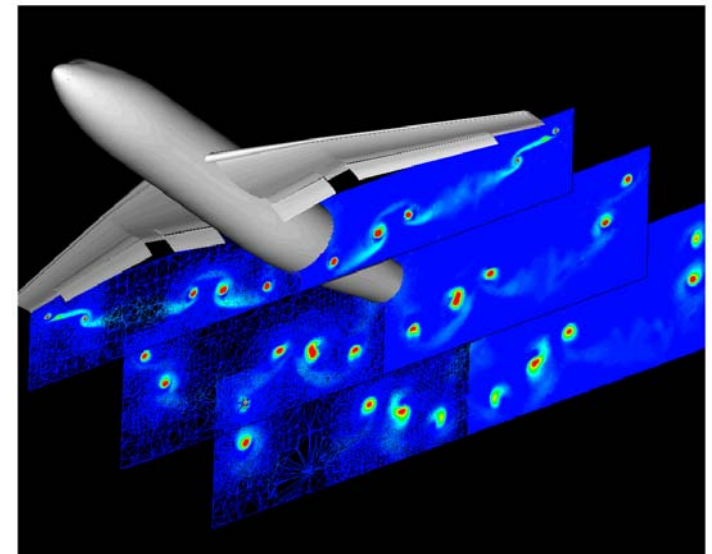
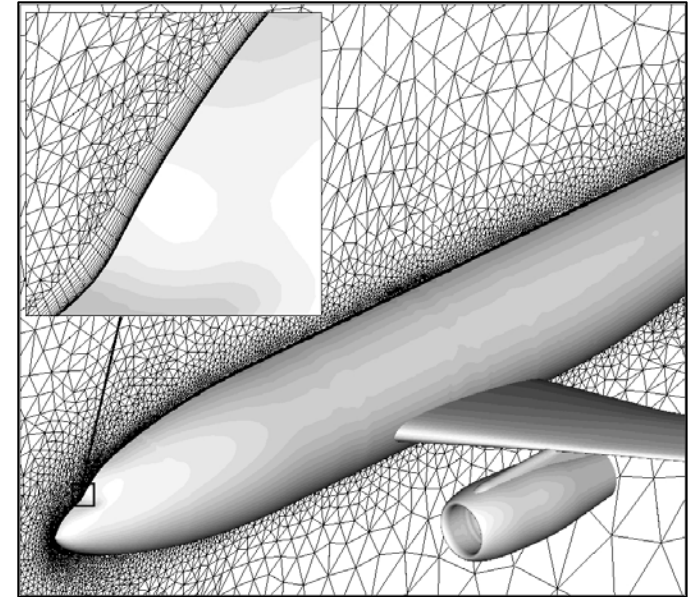
- 3D compressible Navier-Stokes equations
- arbitrarily moving bodies
- steady and time accurate flows
- state-of-the-art turbulence models

## Grid strategy

- unstructured/hybrid grids
- semi-structured sublayers
- overset grids (Chimera)
- deforming grids
- grid adaptation (refinement, de-refinement)

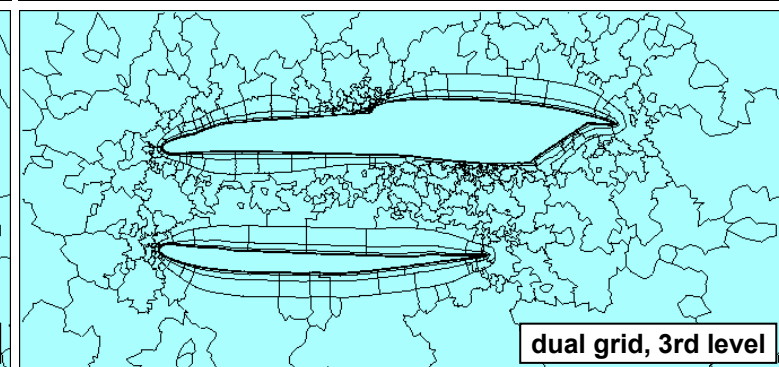
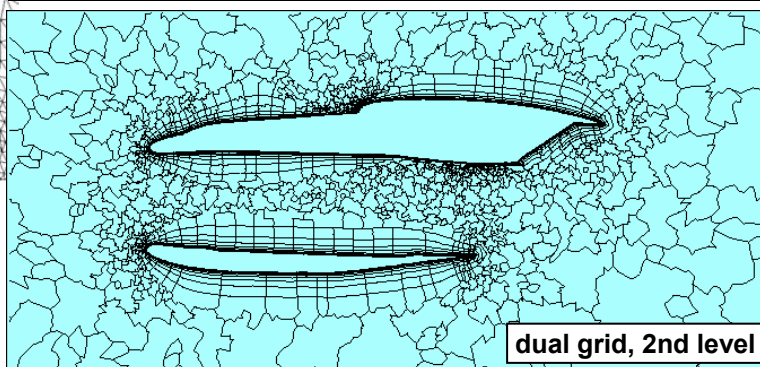
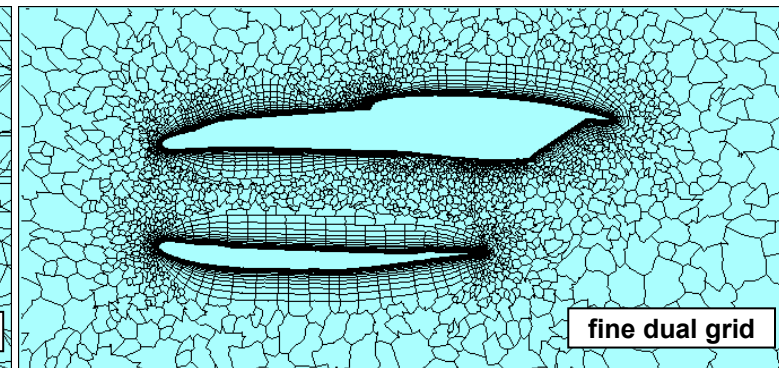
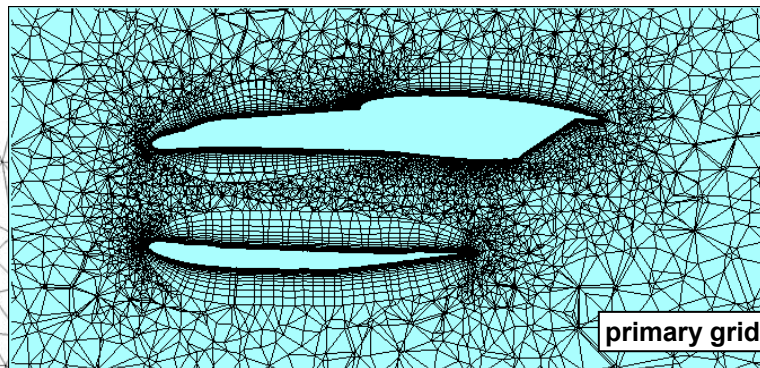
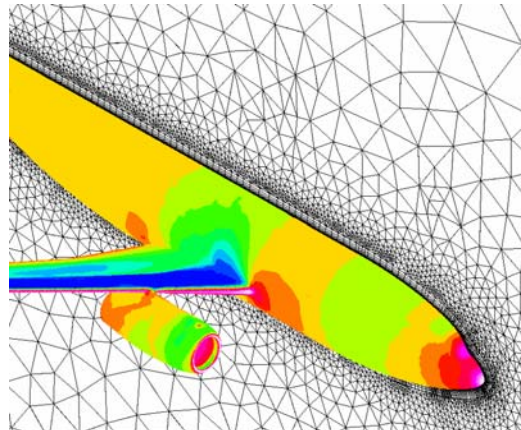
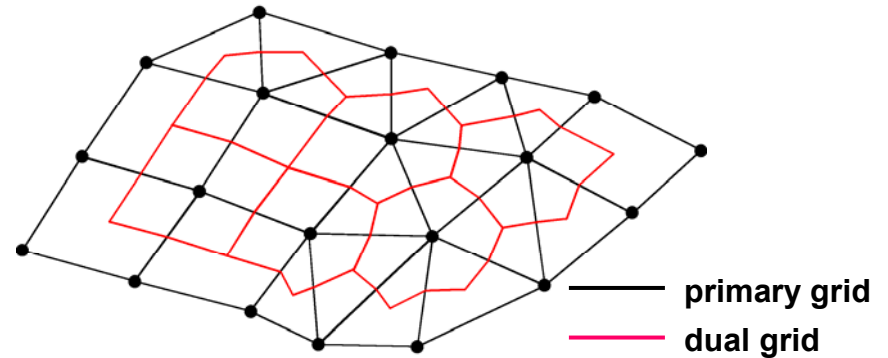
## Numerical algorithms

- 2nd order finite volume discretization based on dual grid approach
- central and upwind schemes
- multigrid based on agglomeration
- implicit schemes for time accurate flows
- preconditioning for low speed flow
- optimized for cash and vector processors
- MPI parallelization



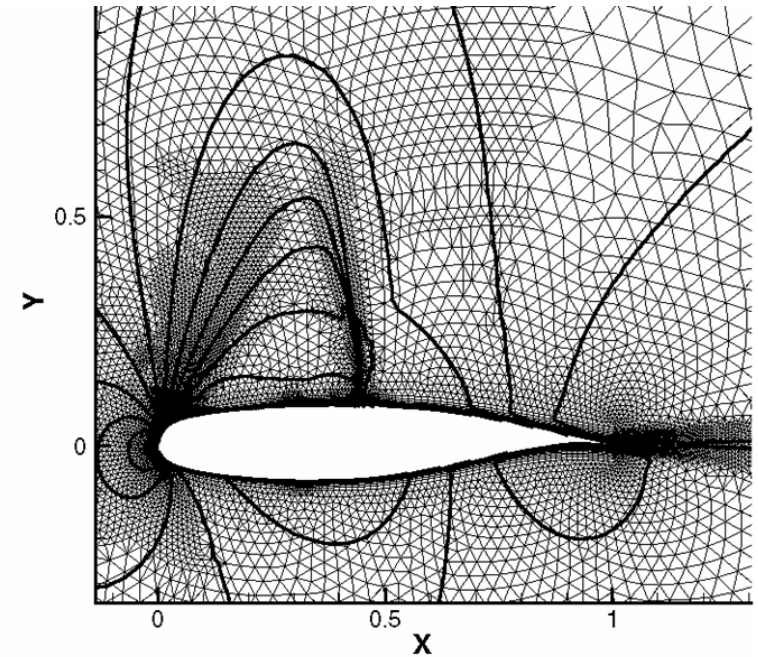
## Dual grid approach

- solver independent of cell types of primary grid
- efficient edge-based data structure
- agglomeration of dual cells for coarser meshes (multigrid)



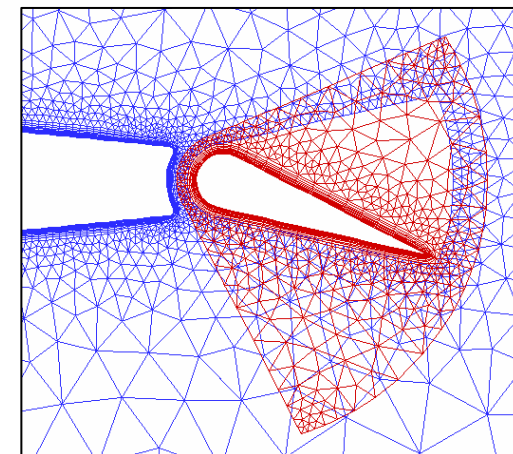
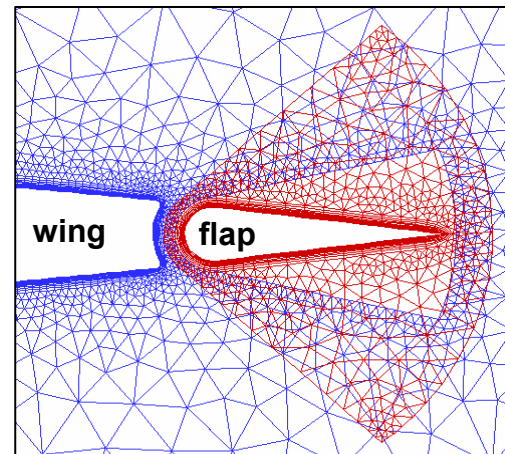
## Local Mesh Adaptation

- local grid refinement and de-refinement depending flow solution
- reduction of total number of grid points
- efficient simulation of complex flow phenomena



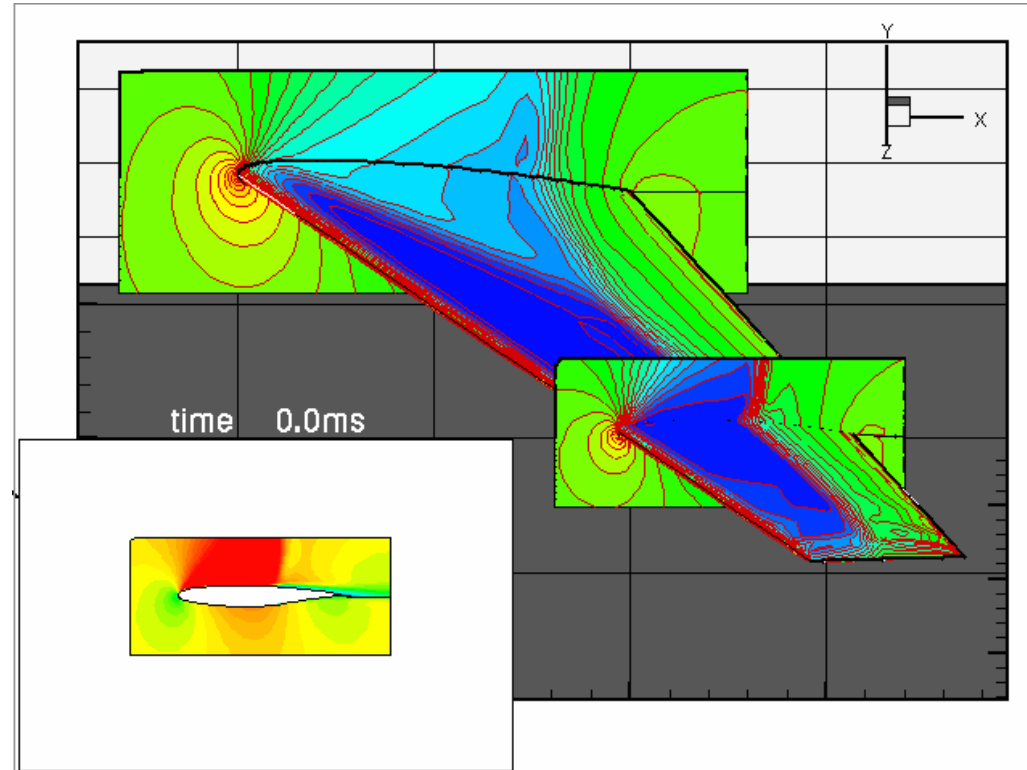
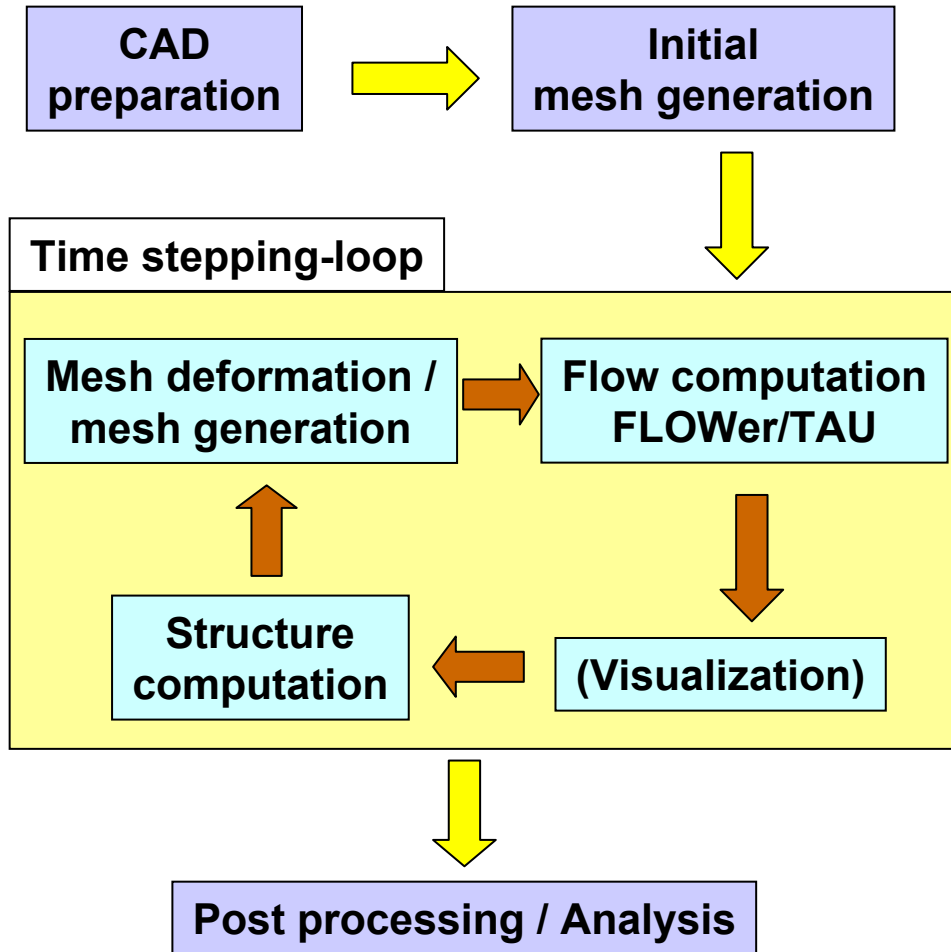
## Overlapping grid technique

- efficient approach for simulation of complex configurations with movable control surfaces (*maneuvering aircraft*)
- separate grids for movable surfaces
- parallel implementation





# Fluid / Structure Coupling

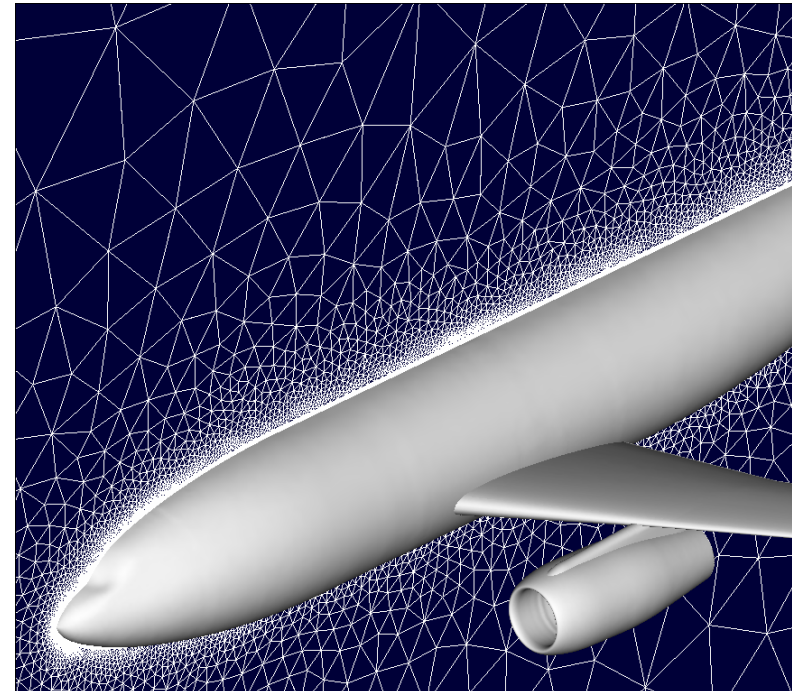
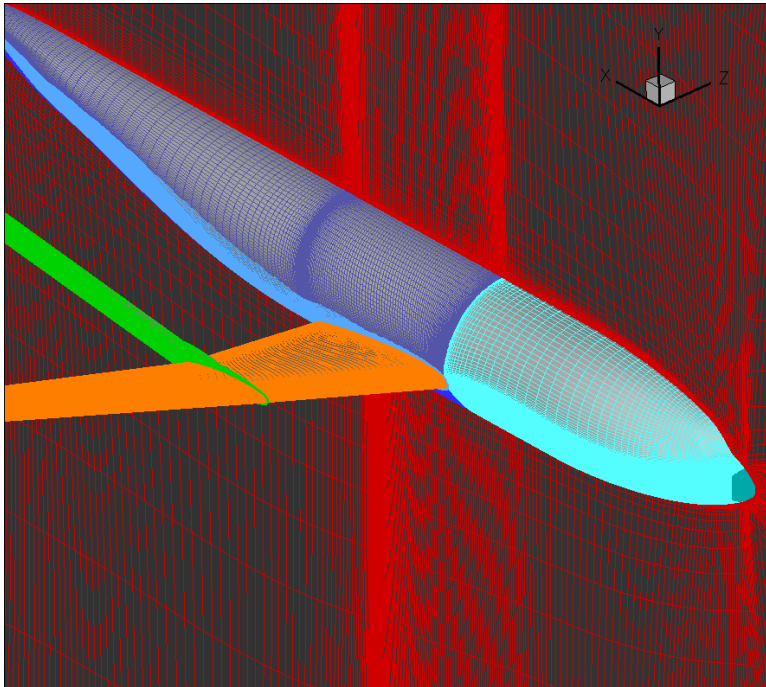


FLOWer



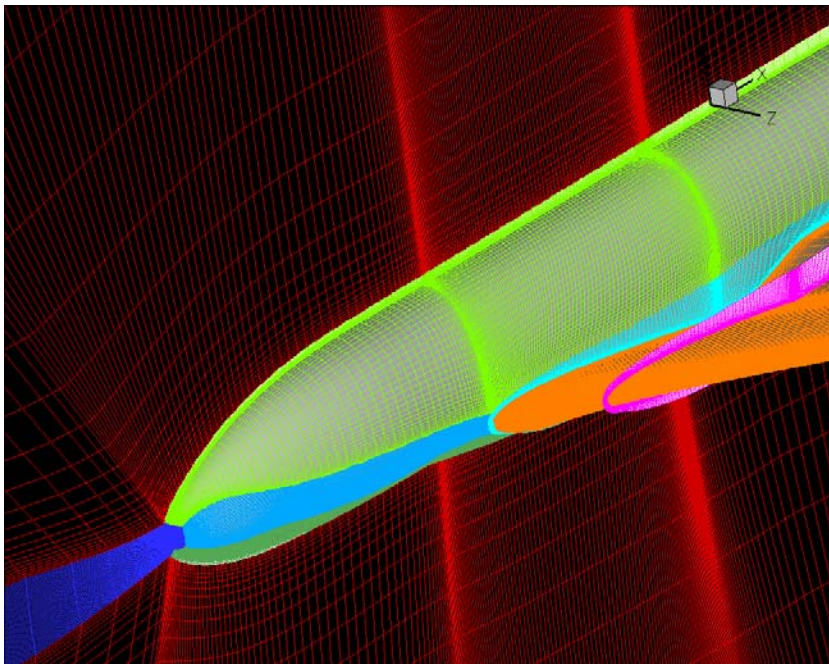
# Validation

- **Aerodynamic performance of wing/body configuration in cruise condition**
- **Engine/airframe integration – installation drag**

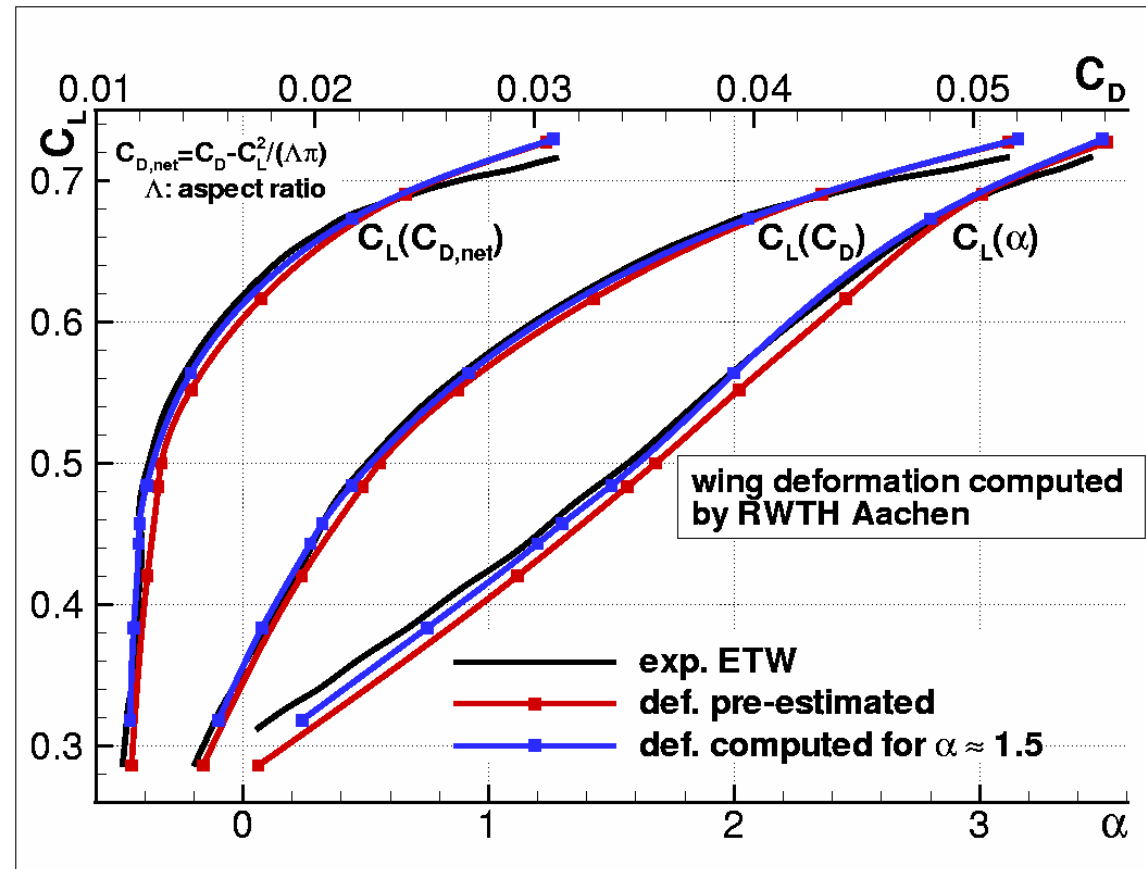


# HiReTT Wing/Body Configuration

- $M_\infty=0.85$ ,  $Re=32.5 \times 10^6$
- coupled CFD/structural analysis for wing deformation at  $\alpha \approx 1.5^\circ$
- FLOWer,  $k\omega$  turbulence model, fully turbulent



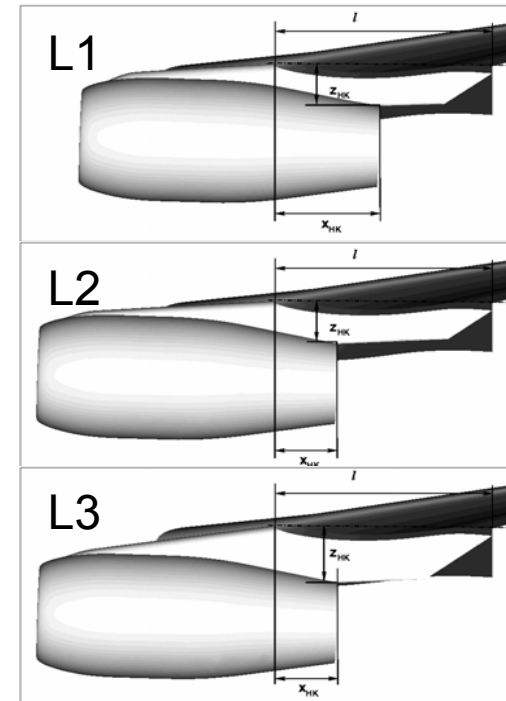
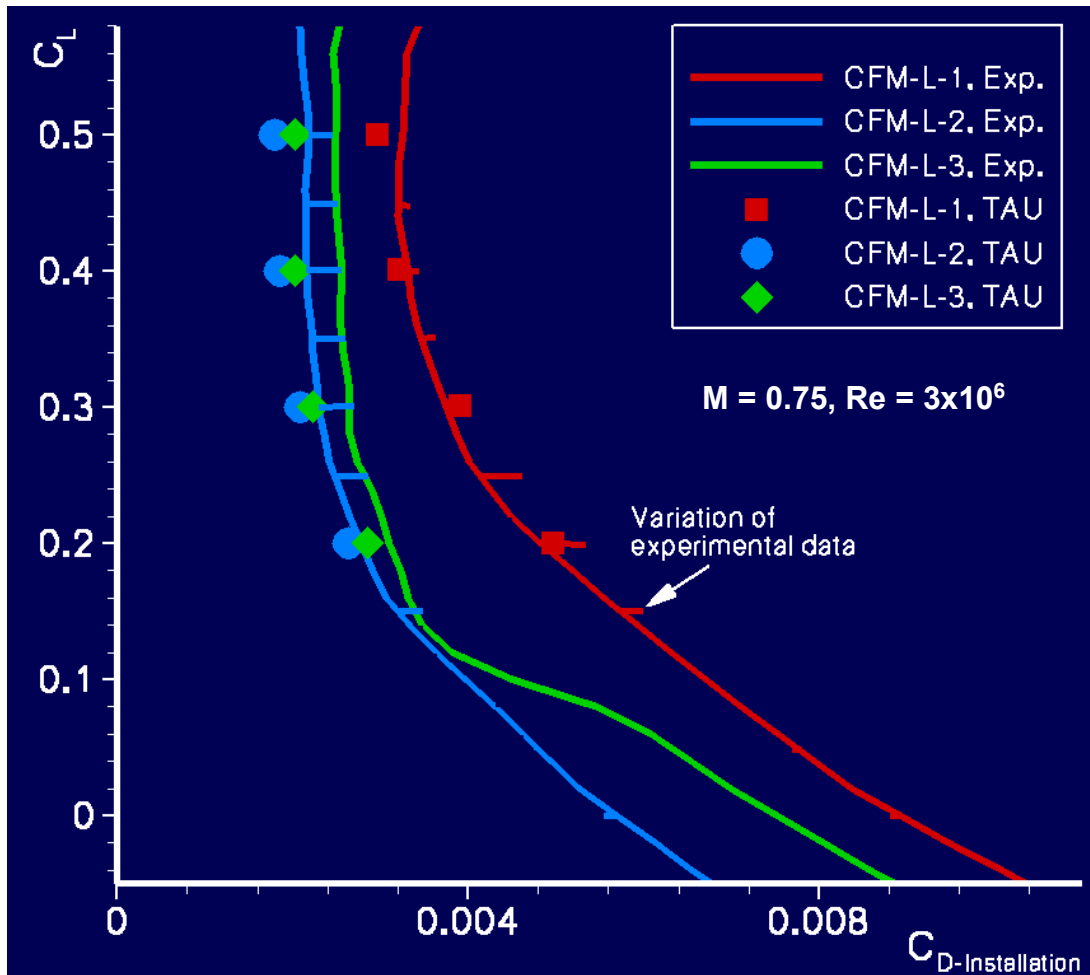
3.5 million grid points



# Engine-Airframe Installation Drag – TAU-Code

**Objective:** Drag prediction for different nacelle positions & shapes

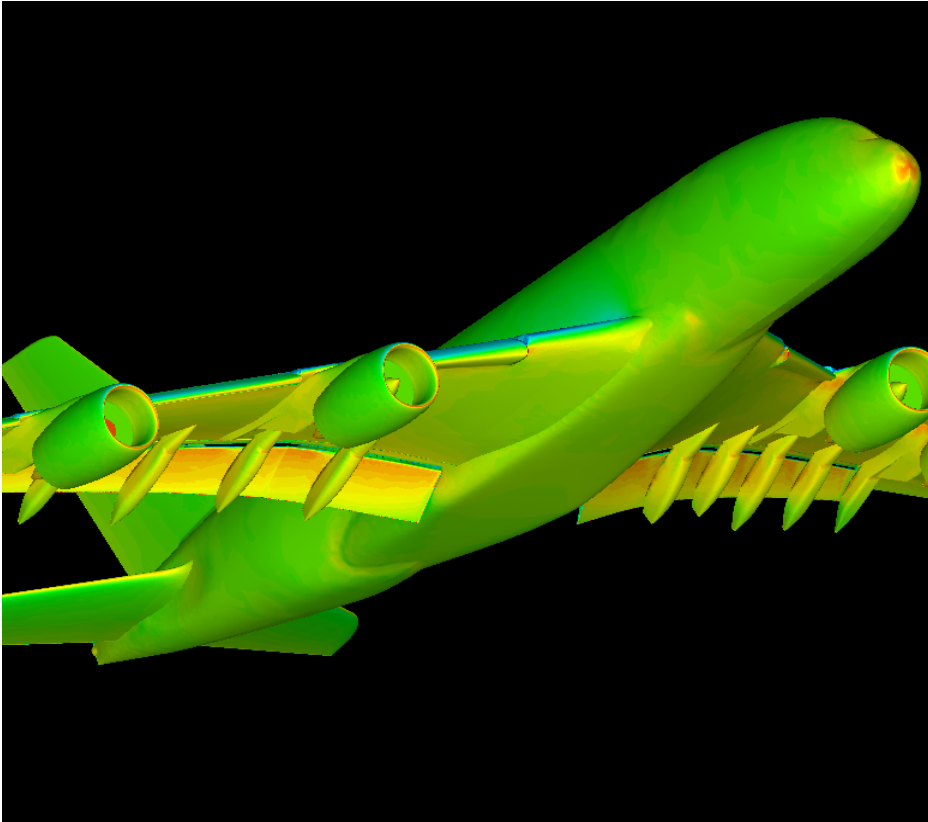
**Configuration:** DLR F6 wing/body/pylon/nacelle configuration



**CFM56**  
(L1,L2,L3,S)

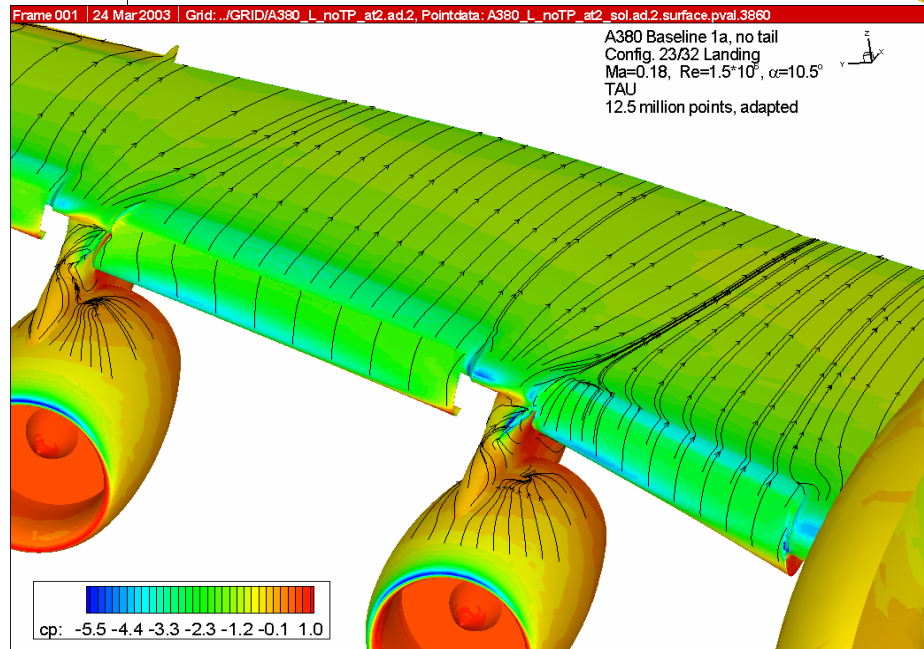
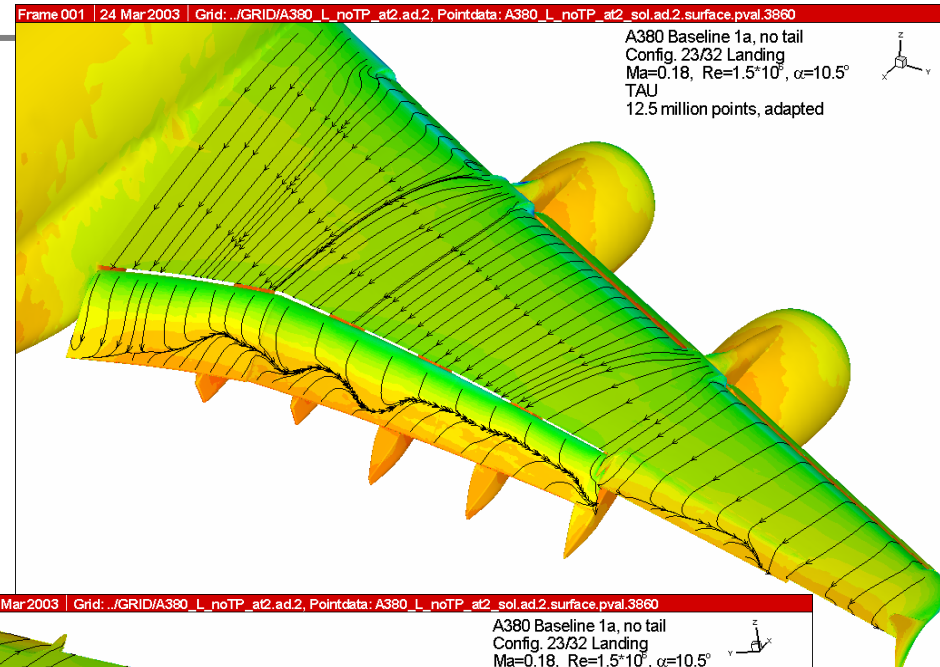
$C_{D-Installation}$	Exp.	CFD
L1 – L2	10.7	11.8
L2 – L3	3.0	2.3

## Airbus A380/800 landing configuration



## TAU computations

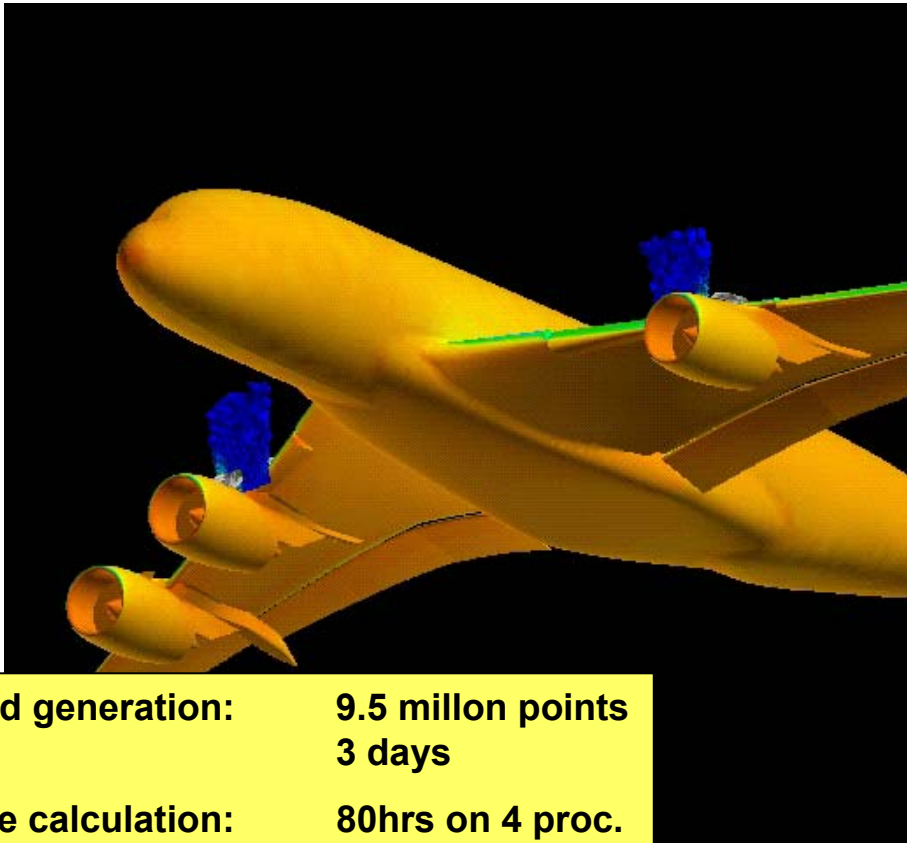
Brodersen



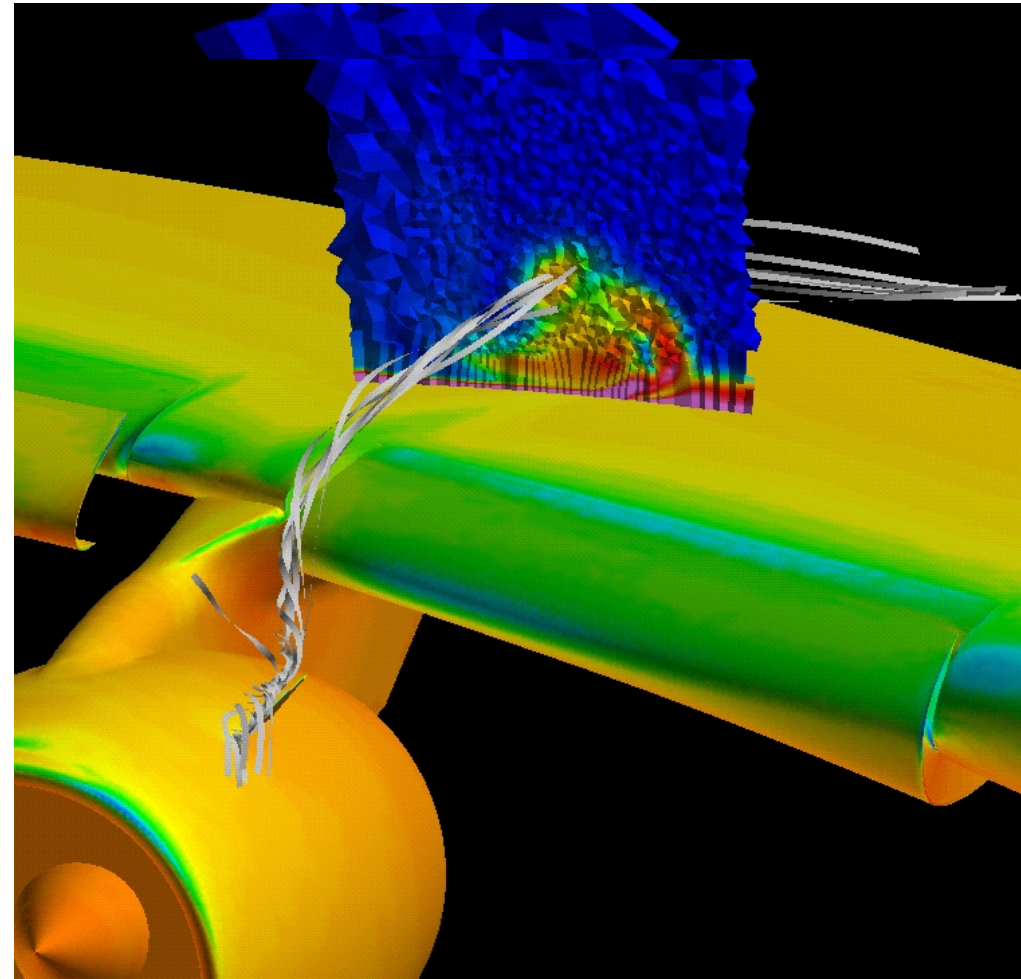


# Complex High- Lift Configurations

**Megaliner landing configuration**  
**Influence of nacelle strakes**



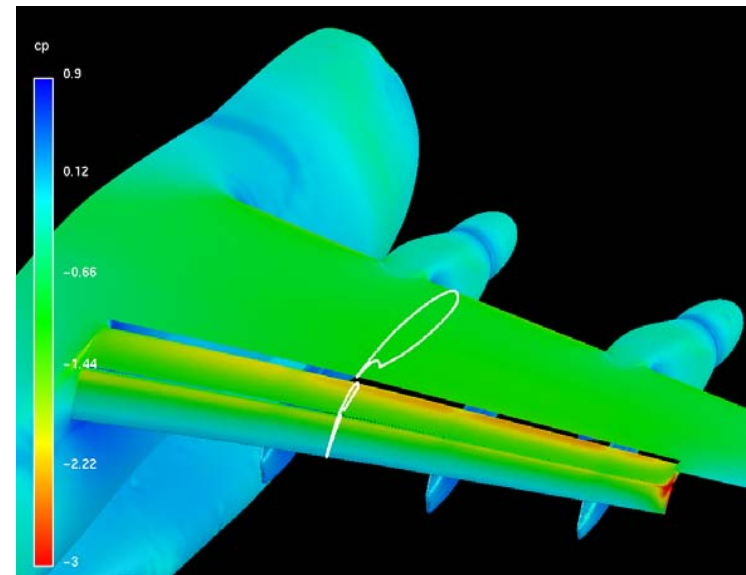
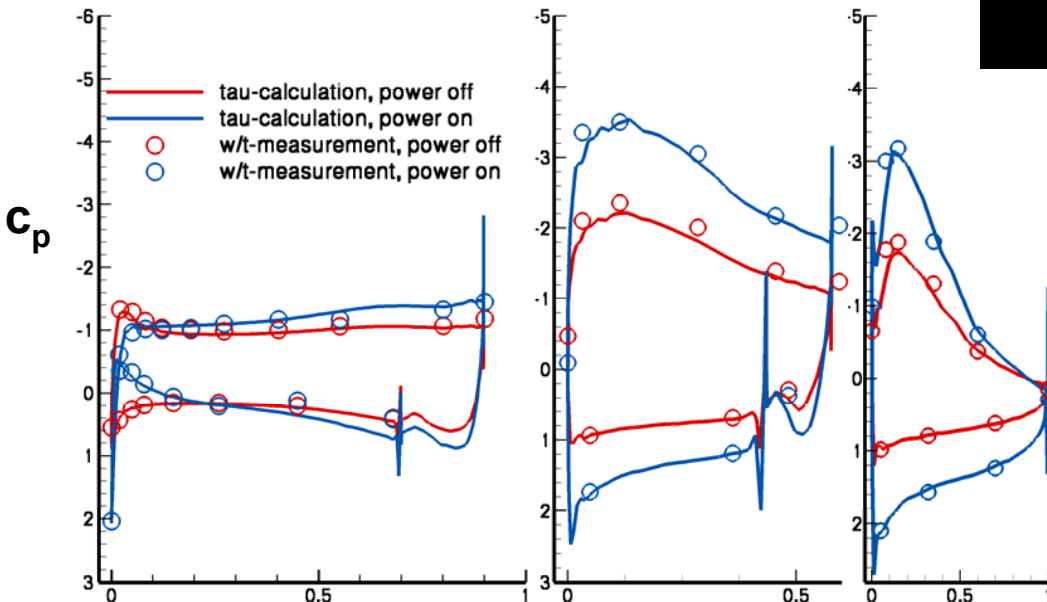
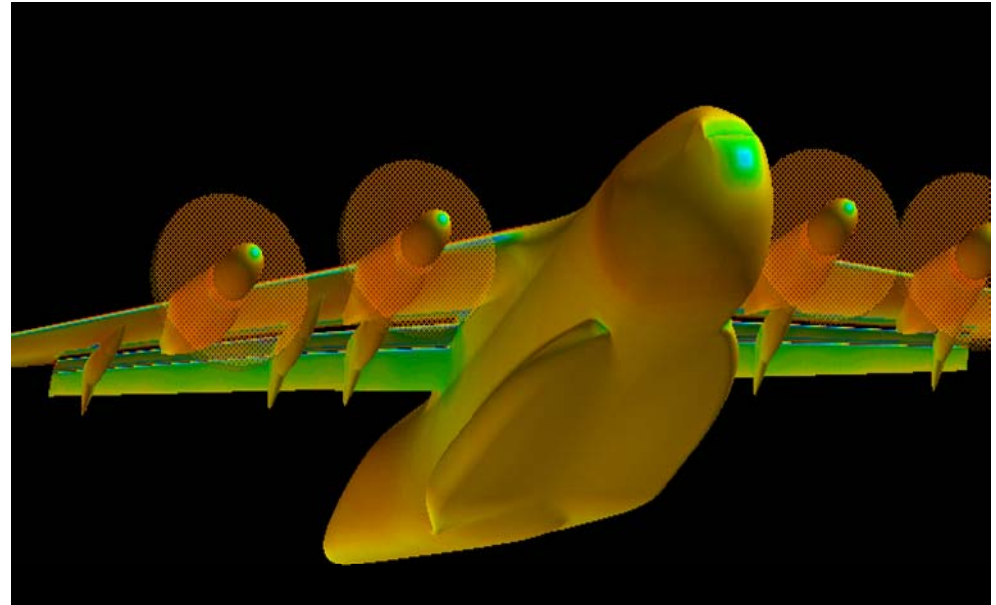
<b>grid generation:</b>	<b>9.5 million points</b> <b>3 days</b>
<b>one calculation:</b>	<b>80hrs on 4 proc.</b> <b>NEC SX5</b>



**TAU computations**

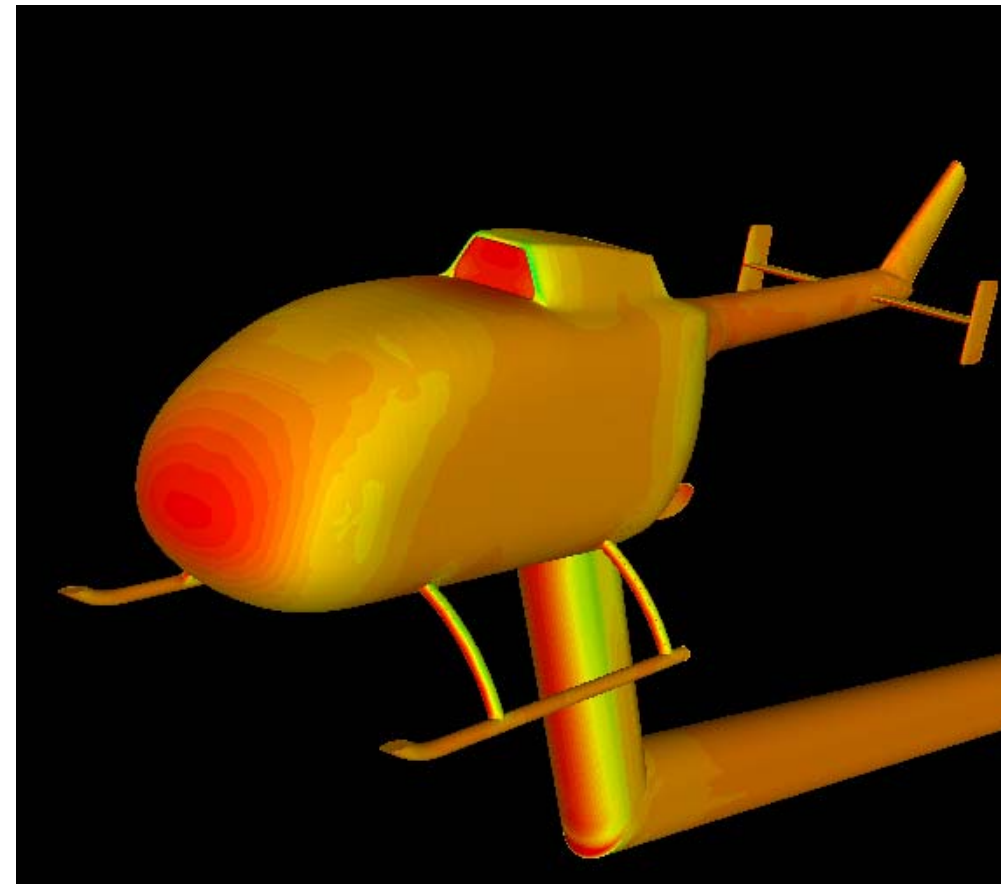
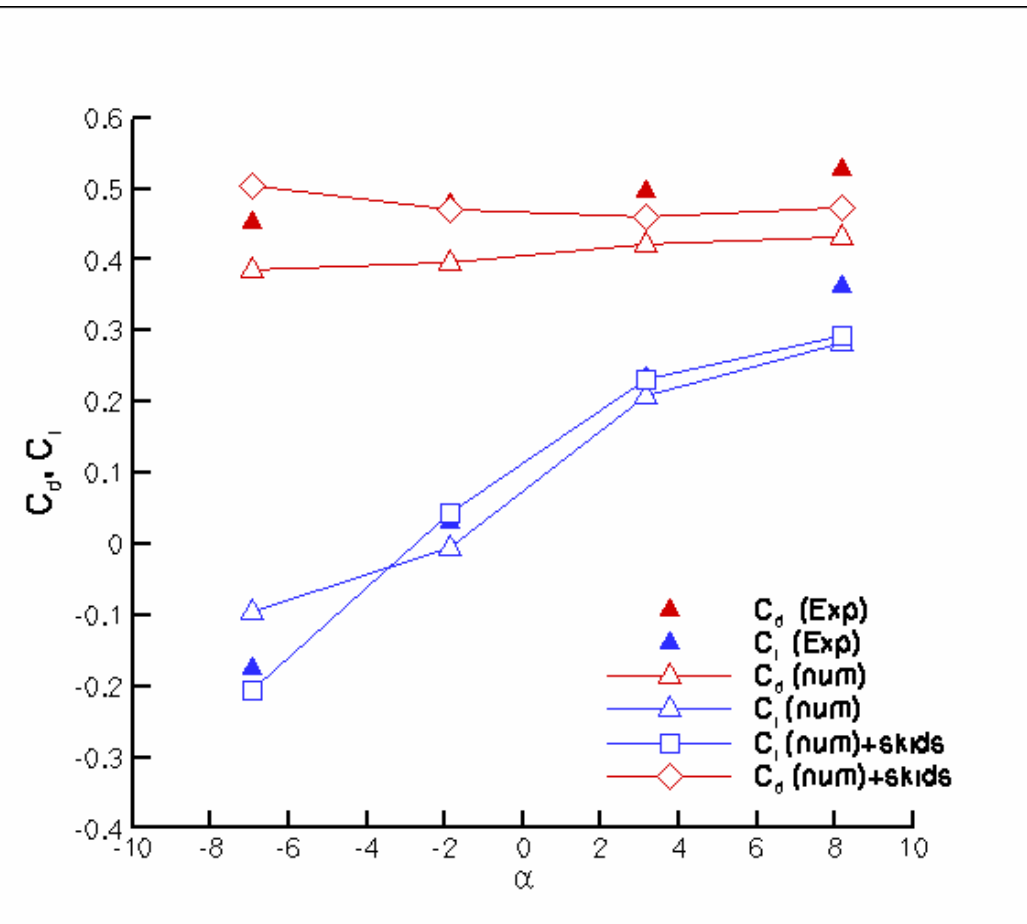
## TAU computation

- hybrid mesh (CENTAUR™)
- 30 prism layers
- 440000 surface points
- $Re = 1.3 \times 10^6$
- $12.9 \times 10^6$  field points



Chimera grid system  
345 blocks, 5.8 mio. grid points

FLOWer Chimera calculation

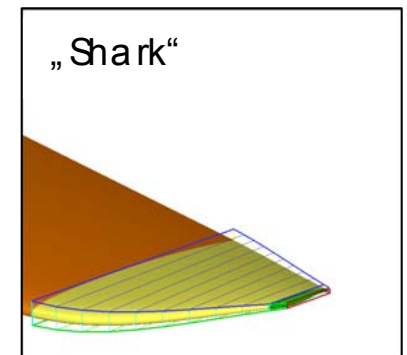
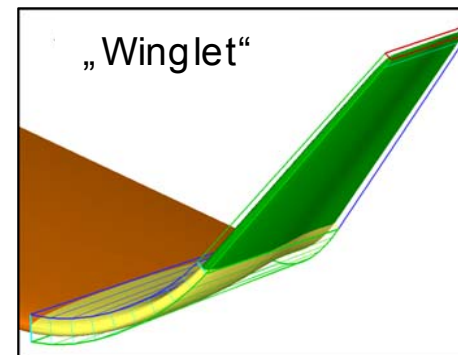
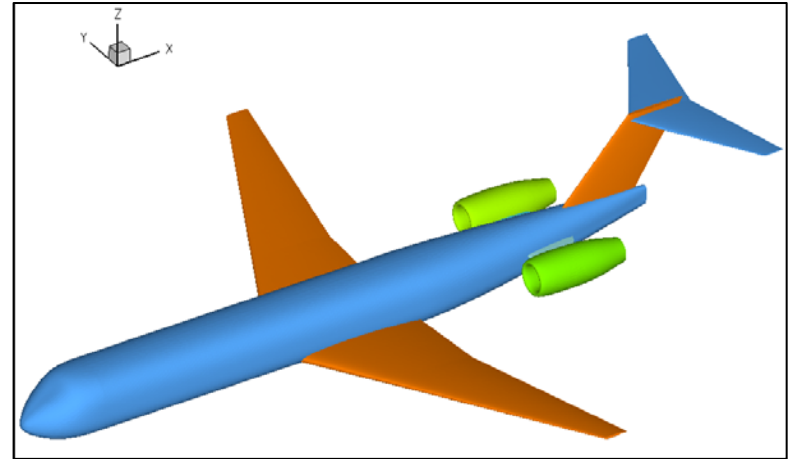


$c_p$ - distribution

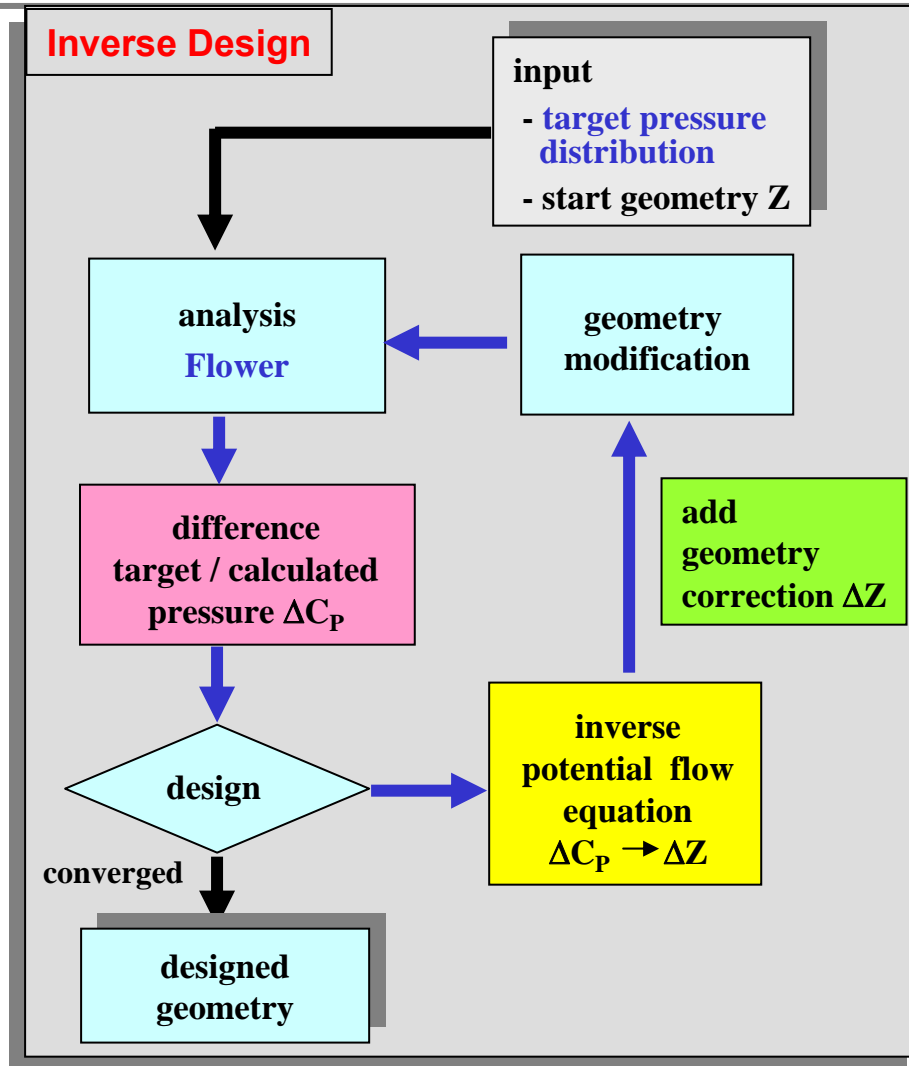


## Design studies by

- analysis of different geometries
- inverse design
- numerical shape optimization



# Inverse Design (FLOWer option)



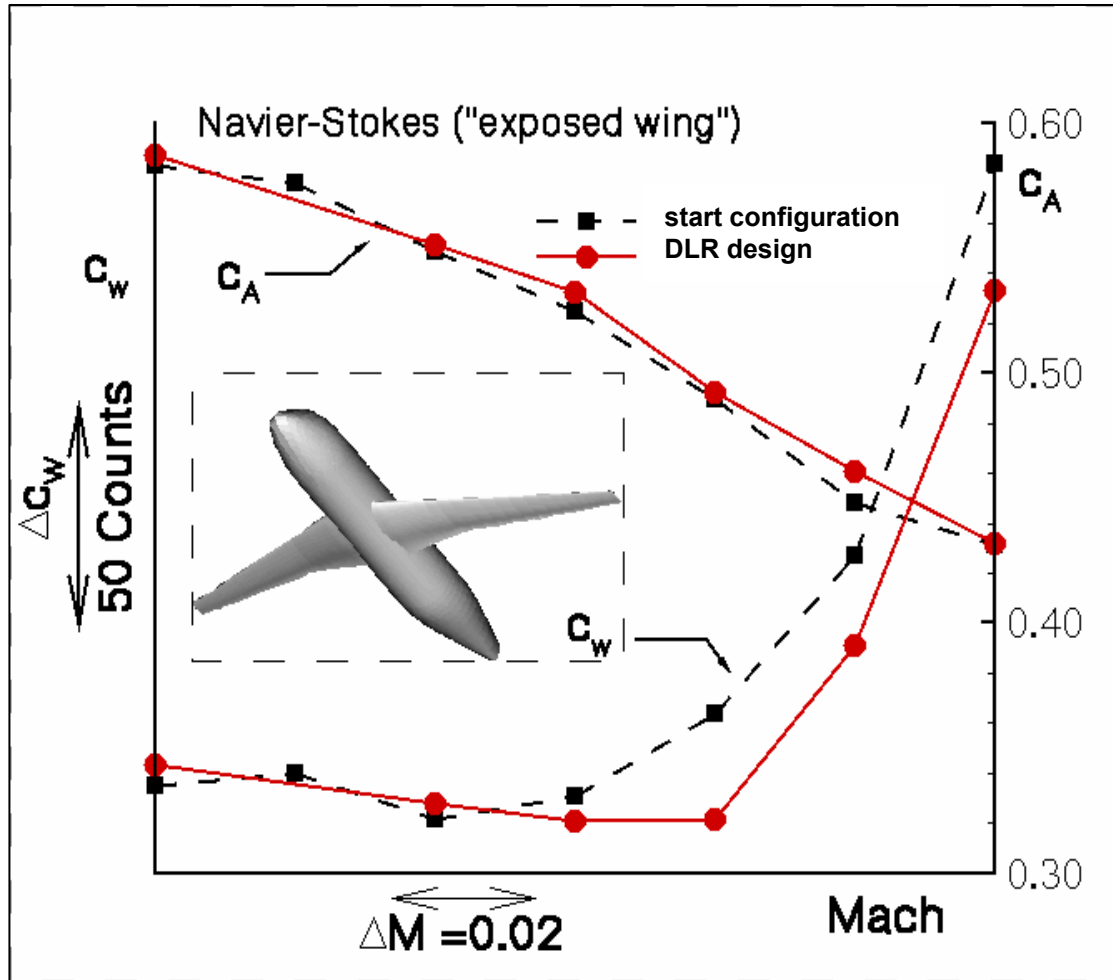
## Inverse method (Bartelheimer/Takanashi)

- pressure difference  $\Delta C_p$  converted to  $\Delta Z$  by solving transonic small perturbation equation (TSP)
- robustness improvement for transonic flow by adding additional damping term
- smoothing of geometry differences  $\Delta Z$  using Bézier curves
- specification of target pressure using GUI (TpEdit)

## Applications

- airfoil
- isolated wing
- isolated nacelle
- wing/body

# Inverse Wing Design



## Objective

- drag rise improvement

## Configuration

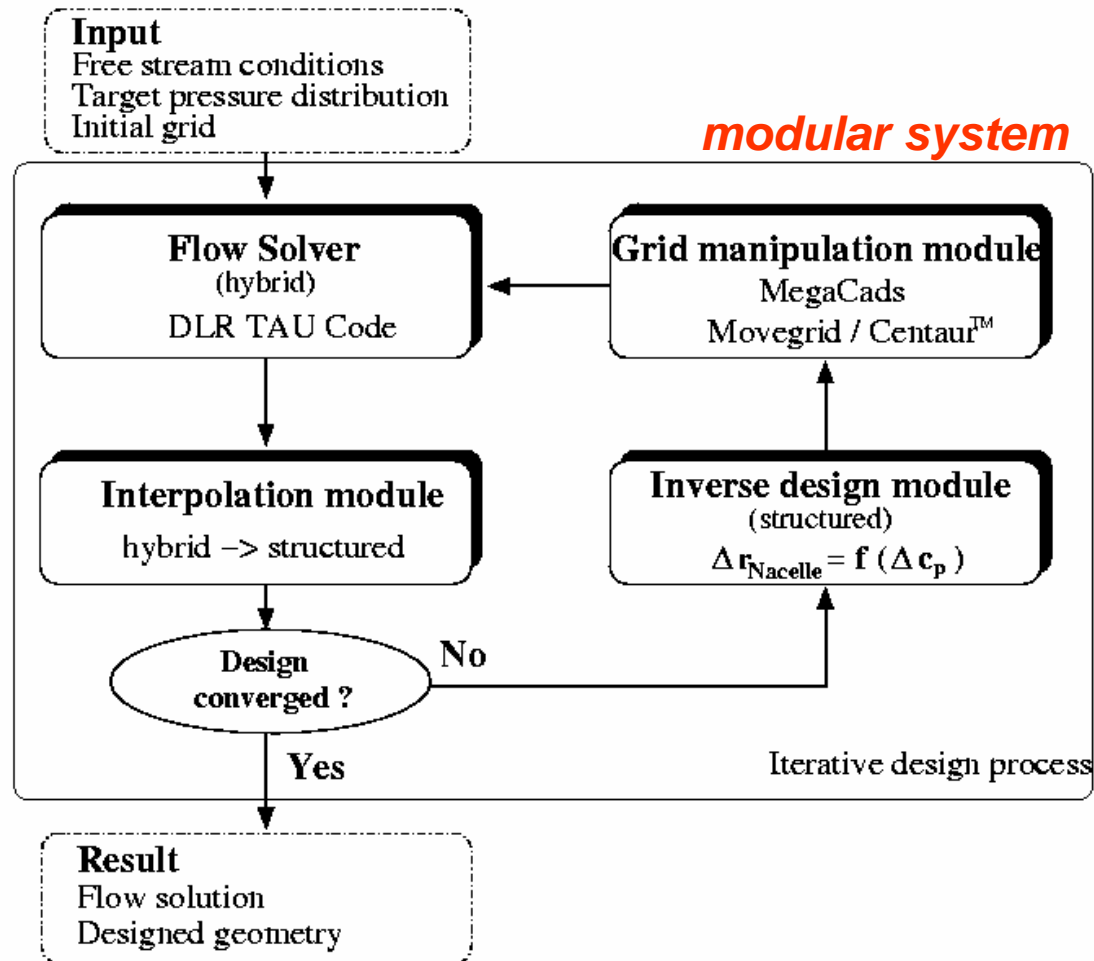
- F/D 728/928 (n=1.0g)

## Flow Solver

- FLOWer, RANS



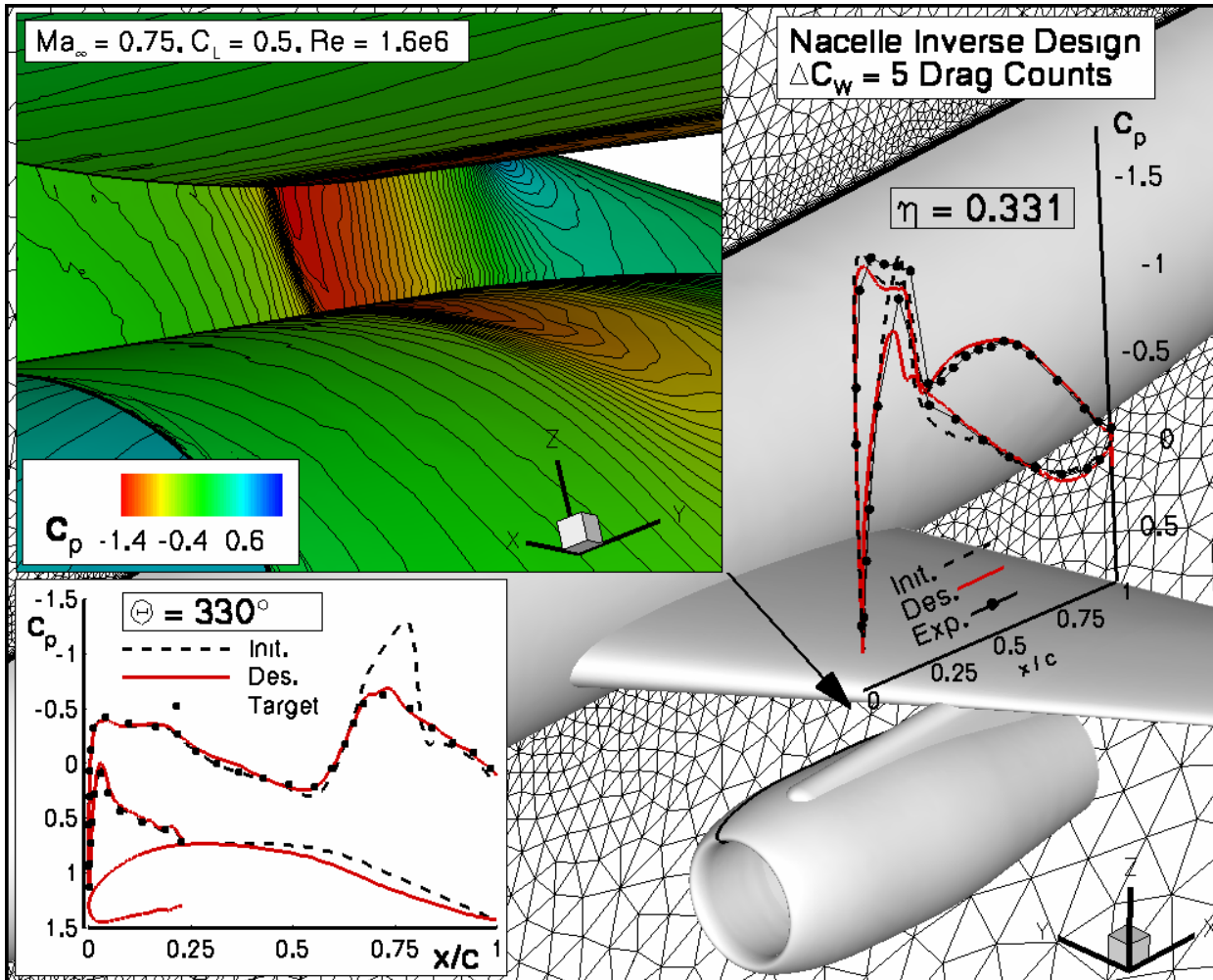
# Integrated Inverse Design System using Tau



## Applications

- isolated nacelle
- integrated nacelle
- integrated empennage design

# Integrated Inverse Nacelle Design



## Objective

- drag reduction through improved nacelle design

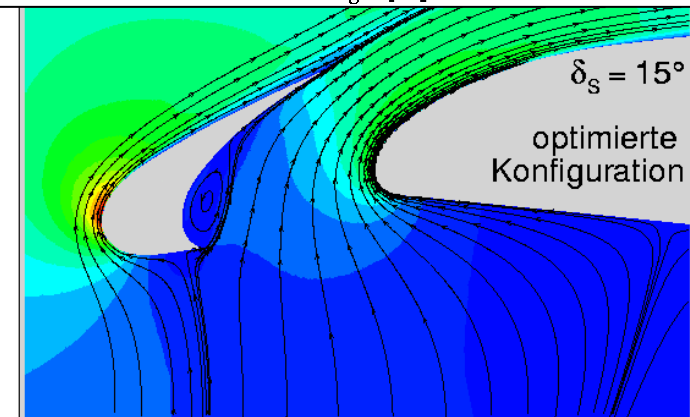
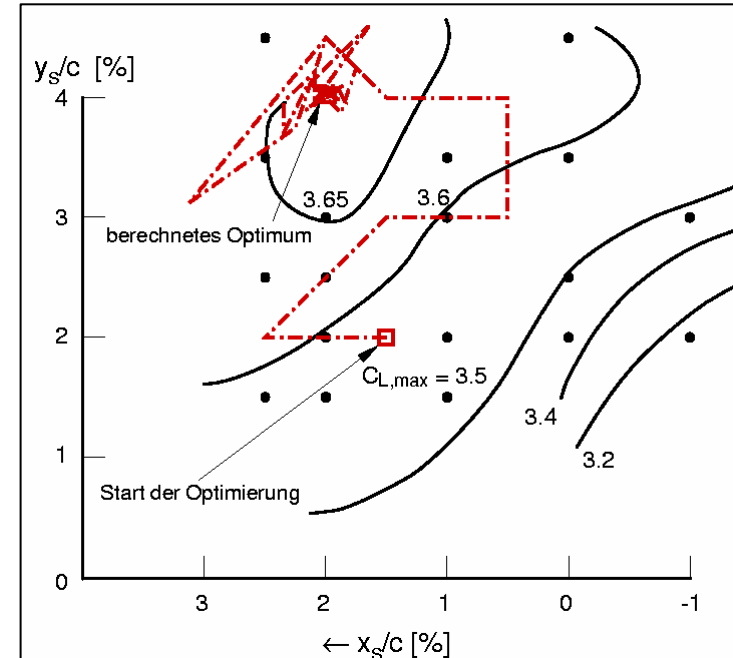
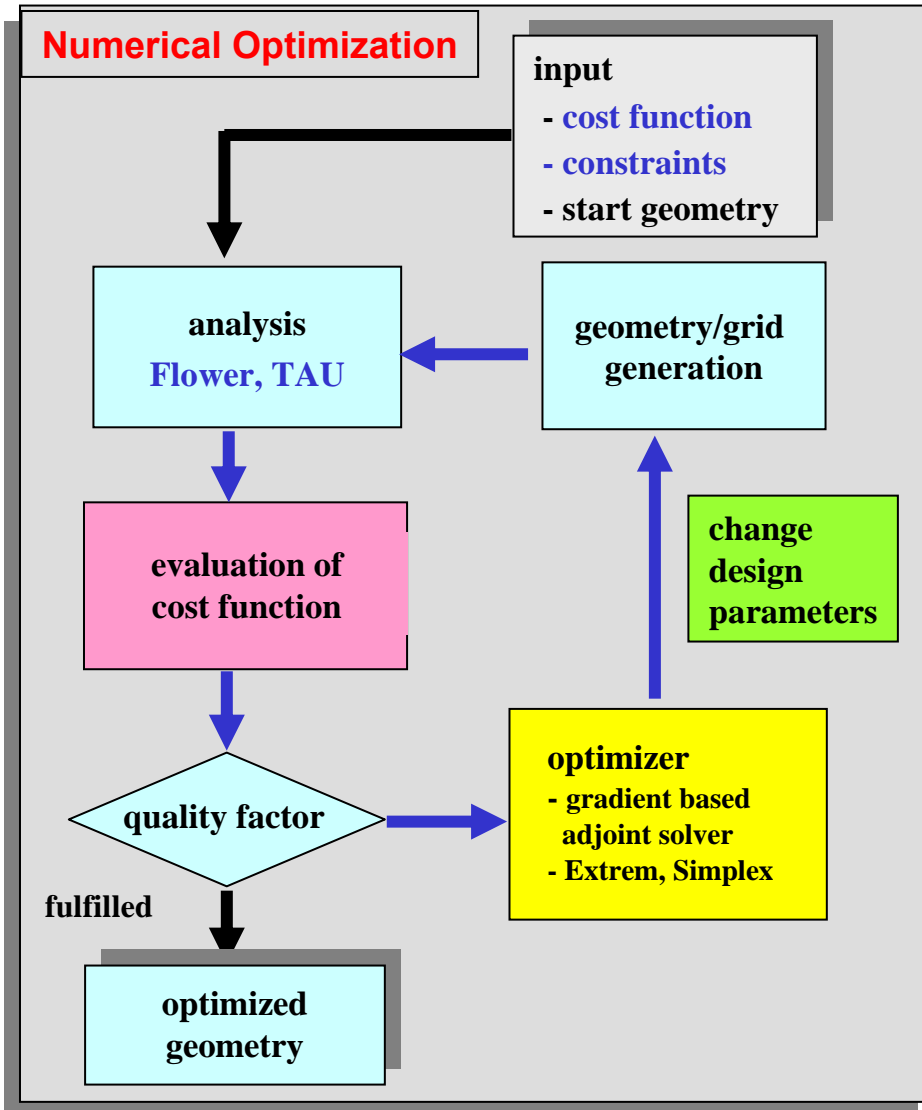
## Configuration

- F6 wing/body/pylon/nacelle
- M=0.75, C<sub>L</sub>=0.5, Re=3 Mil.

## Flow Solver

- TAU, inviscid

# Aerodynamic Shape Optimization



setting optimization,  $C_{a_{max}}$

$M=0.197, Re=3.52 \times 10^6$

# Numerical Optimization of High-Lift 3-Element Airfoil

single point, single discipline, single objective

## Application

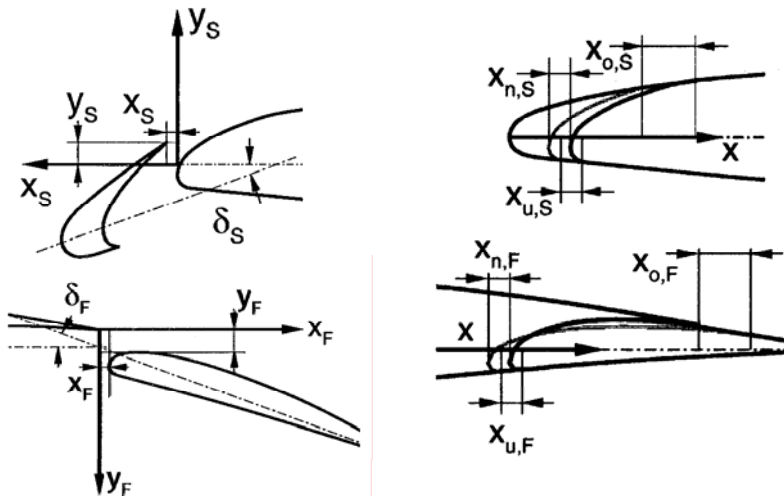
- drag optimization for 3-element airfoil
- take-off configuration ( $M_\infty=0.2$ ,  $Re=3.52 \times 10^6$ )

## Cost function:

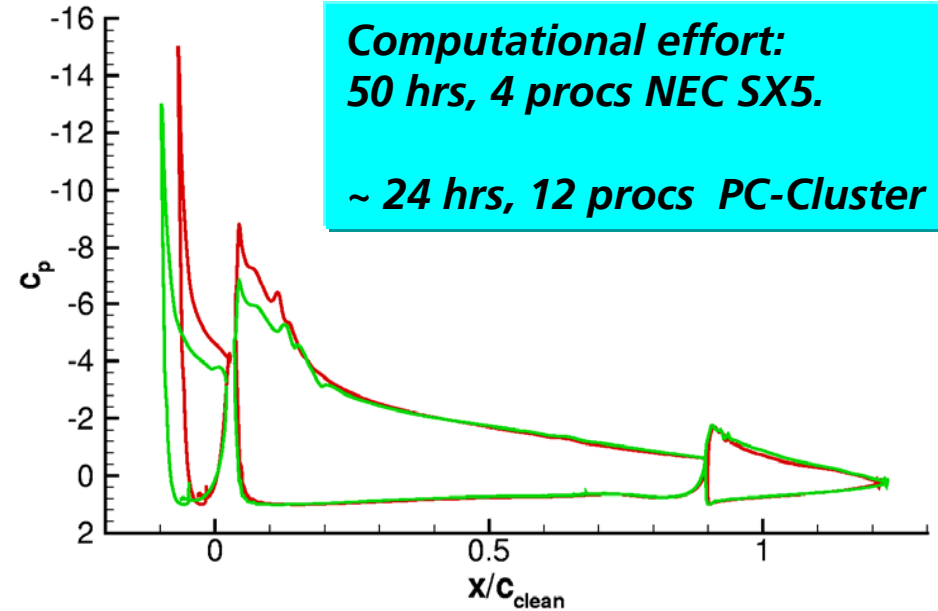
- minimum drag with constant lift and constraint pitching moment

## Design parameters (12)

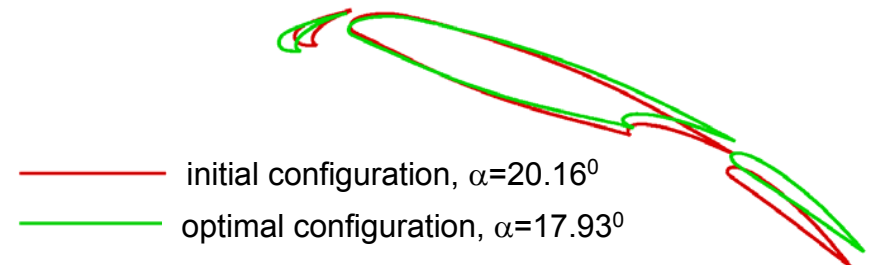
- element position & deflection
- element-size variations



pressure distribution



**Computational effort:**  
50 hrs, 4 procs NEC SX5.  
~ 24 hrs, 12 procs PC-Cluster



— initial configuration,  $\alpha=20.16^\circ$   
— optimal configuration,  $\alpha=17.93^\circ$



## Requirements

- multi-point design, multi-objective optimization, multi-disciplinary optimization
- large number of design variables
- physical and geometrical constraints
- complex configurations
- parametrization based on CAD model
- meshing & mesh deformation techniques ensuring grid quality
- compressible Navier-Stokes equations with accurate models for turbulence and transition
- validated and efficient CFD codes
- efficient & reliable optimization algorithms

## Key elements

- **Geometry parametrization**
- **Meshing & mesh movements methods**
- **Flow solver efficiency & accuracy**
- **Optimization techniques**
- **Multi-disciplinary optimization**
- **Optimization process chain**
- **Verification & Validation**

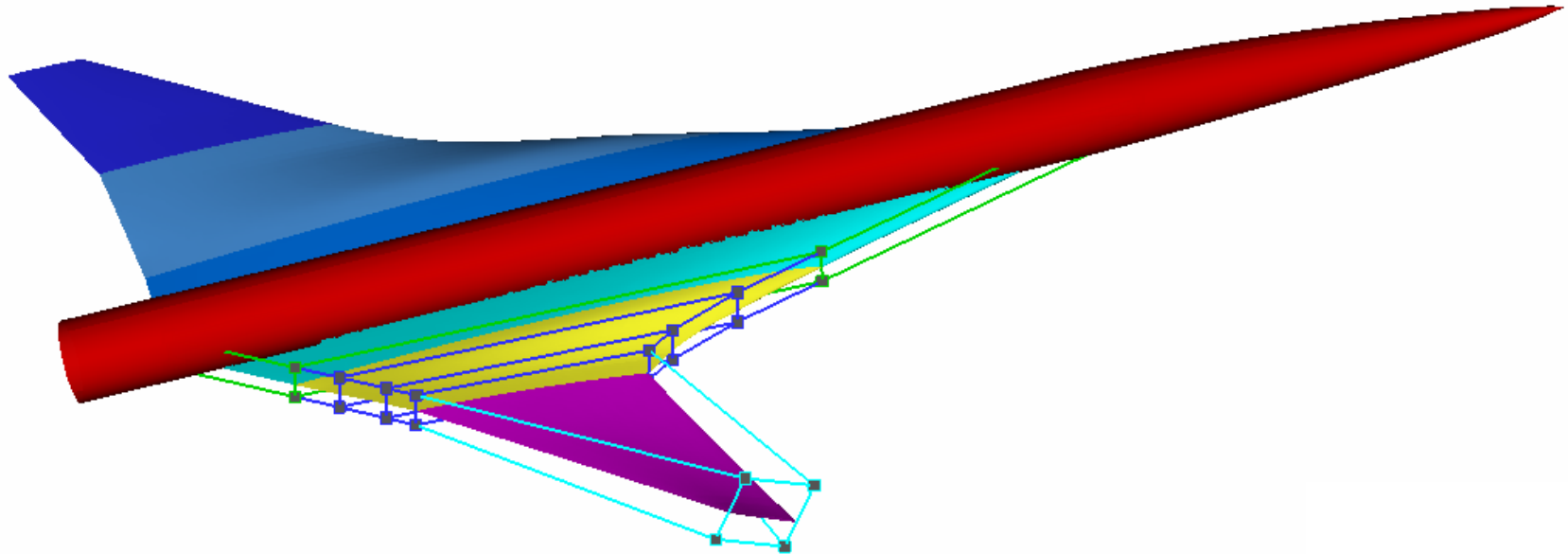
## Main objectives

- Improvement of aircraft shape optimization tools
- Establishment of numerical shape optimization within industrial aircraft design process
- Concentration of activities & resources from DLR, universities, aeronautical industry & SMEs

## Partners

- Airbus-G, EADS-M
- DLR
- CLE, *FastOpt*, Synaps
- Universities of Aachen, Berlin, Braunschweig, Darmstadt, Trier





## Freeform Deformation (FFD)

- parameterization of complex non parametric CAD-based shapes
- high flexibility in combination with grid generation techniques
- widely used for “Soft-Object Animation”

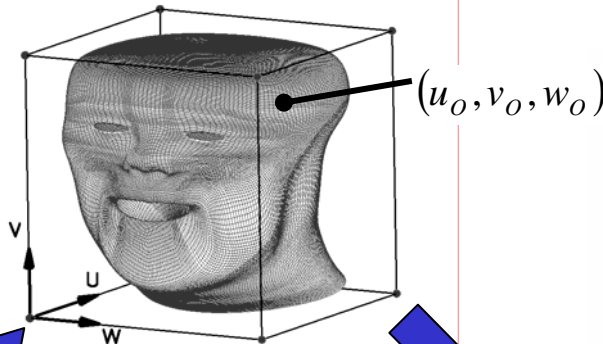
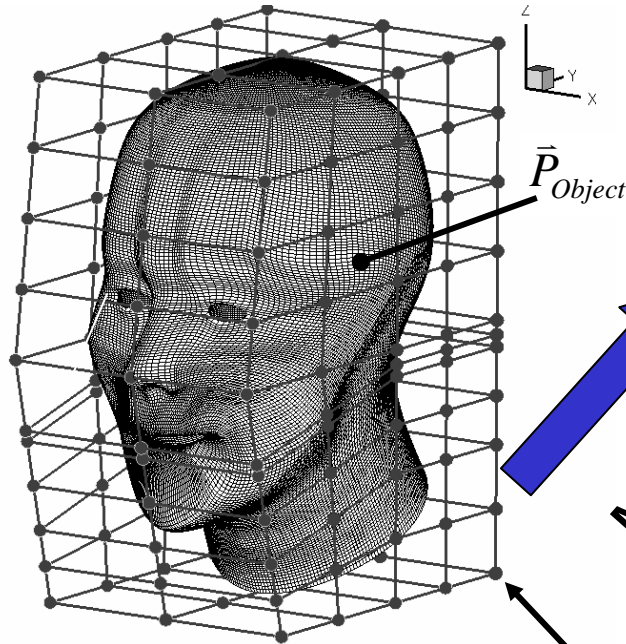
### Idea:

- use FFD as geometry modeler within aerodynamic shape optimization

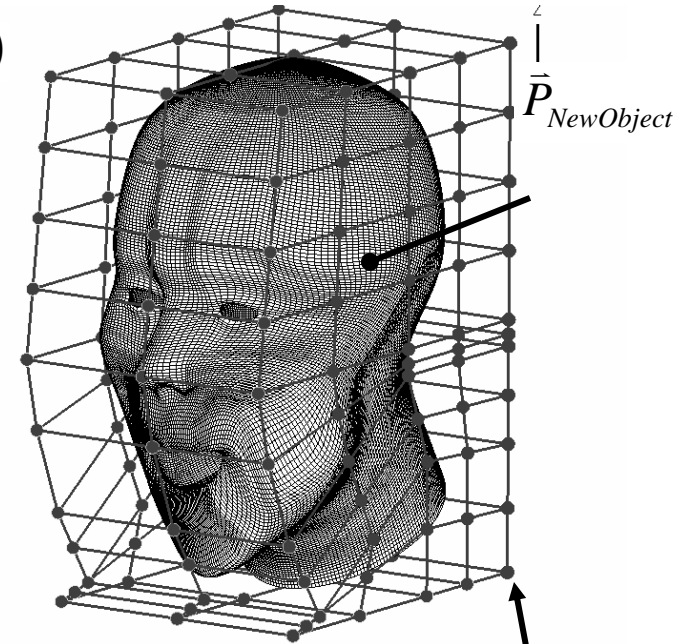


# Freeform Deformation Technique (Sederberg, Parry)

Base-Lattice



Deformation-Lattice



Mapping

Re-Mapping

Evaluate  $(u_o, v_o, w_o)$  from:

$$\bar{P}_{Object}(u_o, v_o, w_o) =$$

$$\sum_{i=0}^{n_u} \sum_{j=0}^{n_v} \sum_{k=0}^{n_w} N_{i,m_u}(u_o) N_{j,m_v}(v_o) N_{k,m_w}(w_o) \bar{Q}_{i,j,k}$$

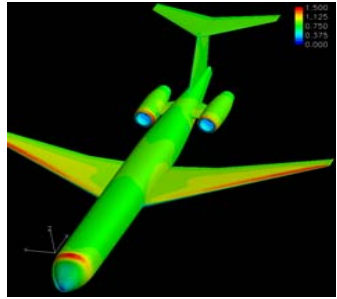
Evaluate  $\bar{P}_{NewObject}$  from:

$$\bar{P}_{NewObject}(u_o, v_o, w_o) =$$

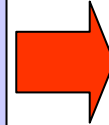
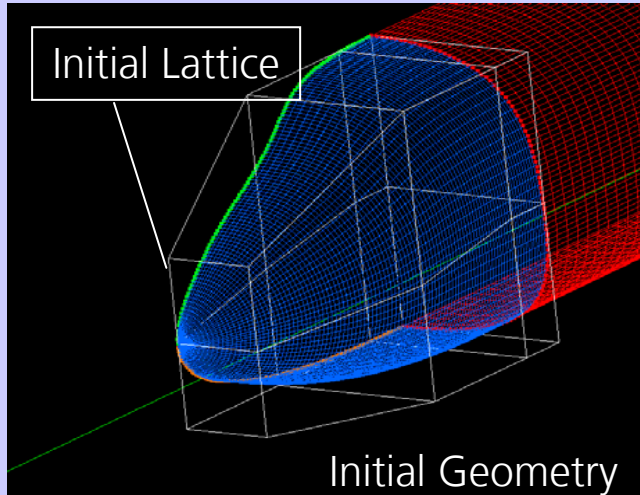
$$\sum_{i=0}^{n_u} \sum_{j=0}^{n_v} \sum_{k=0}^{n_w} N_{i,m_u}(u_o) N_{j,m_v}(v_o) N_{k,m_w}(w_o) \bar{R}_{i,j,k}$$

B-Spline Base Functions:  $N_{i,m_u}(u), N_{j,m_v}(v), N_{k,m_w}(w)$  B-Spline Control Poins:  $\bar{Q}_{i,j,k}, \bar{R}_{i,j,k}$

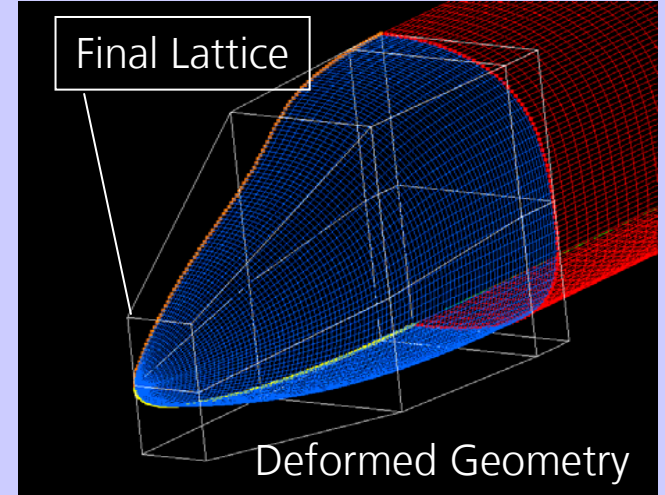
# Principle Steps of Freeform Deformation



Mapping of Geometry into Initial B-Spline Volume

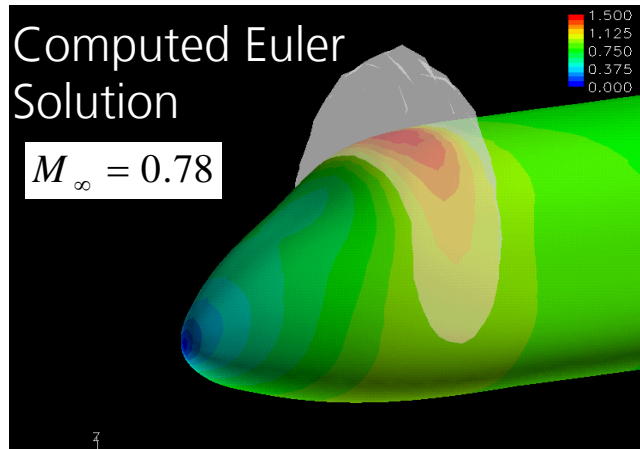


Re-Mapping of Geometry from Final B-Spline Volume



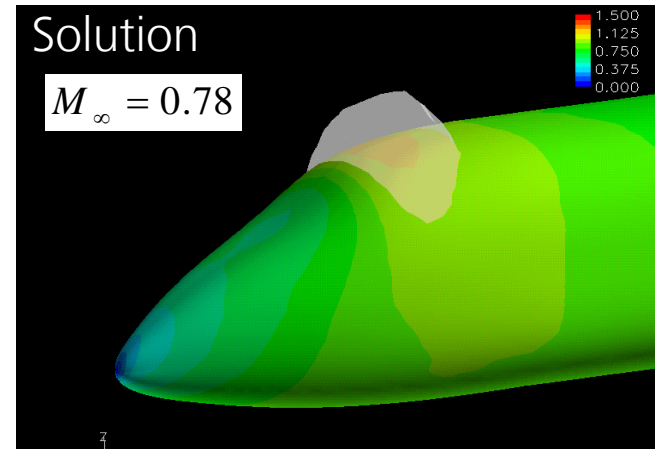
Computed Euler Solution

$M_\infty = 0.78$

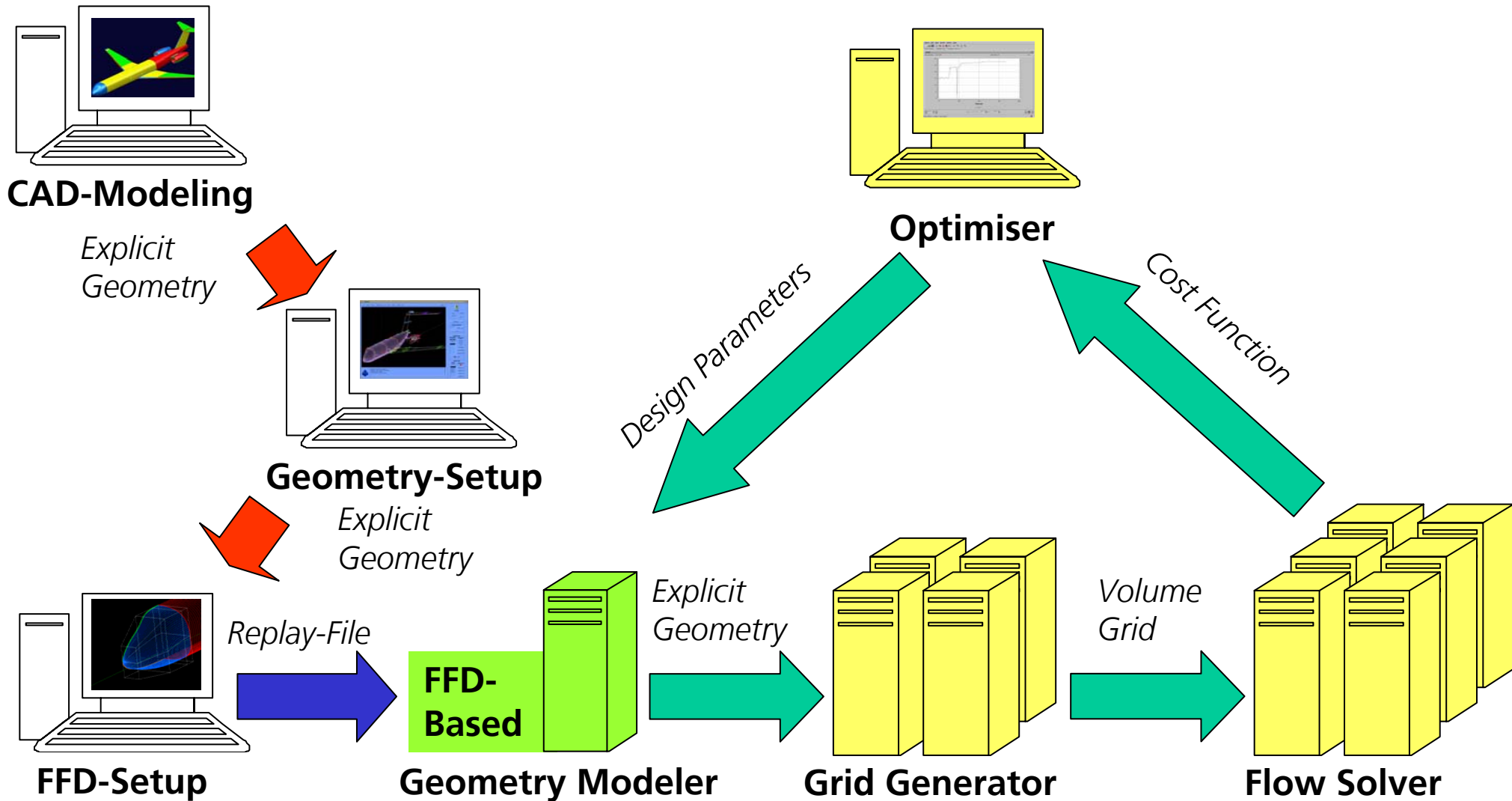


Solution

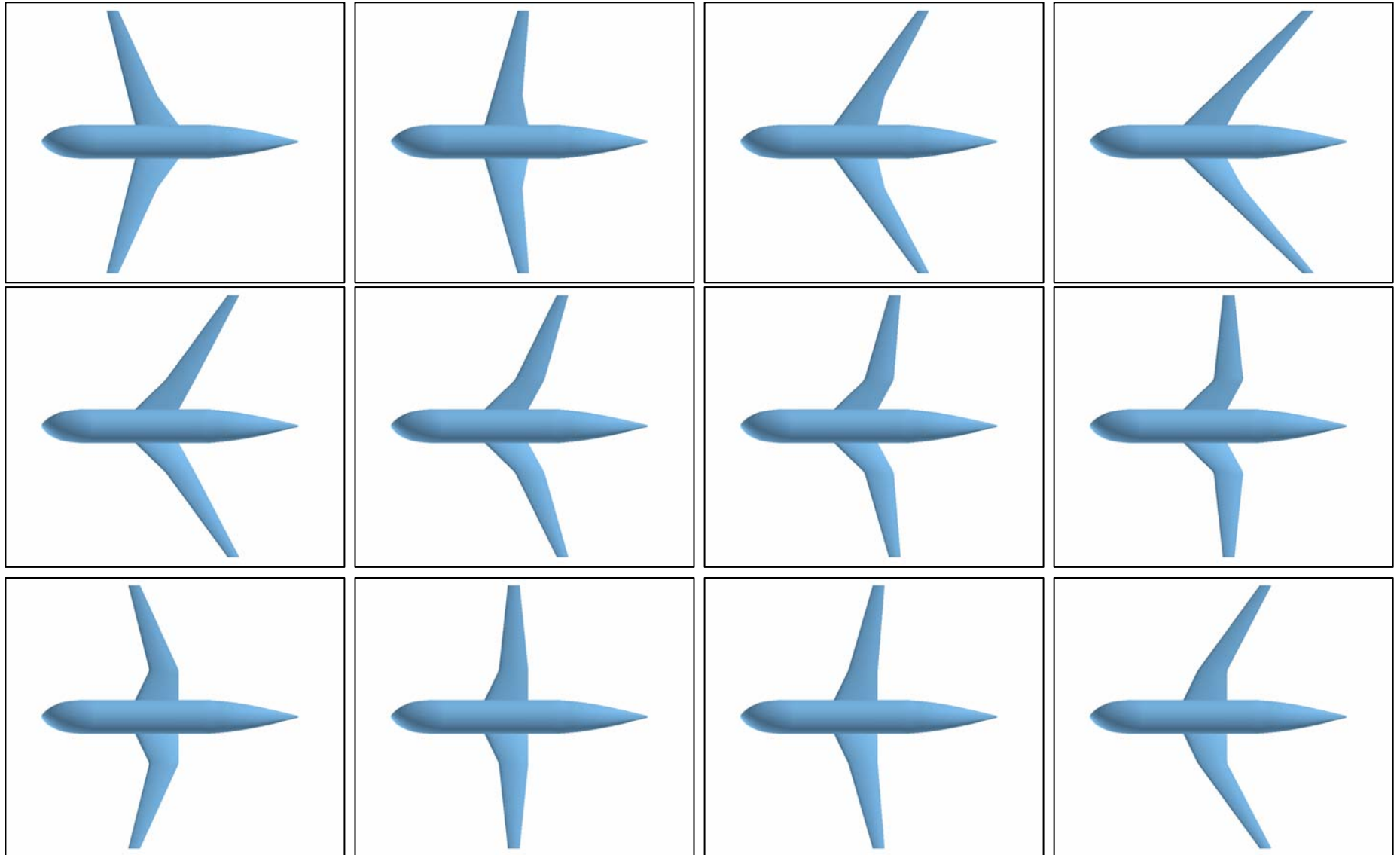
$M_\infty = 0.78$



# Parametric CAD in Aerodynamic Shape Optimization



# Example fro Freeform Deformation



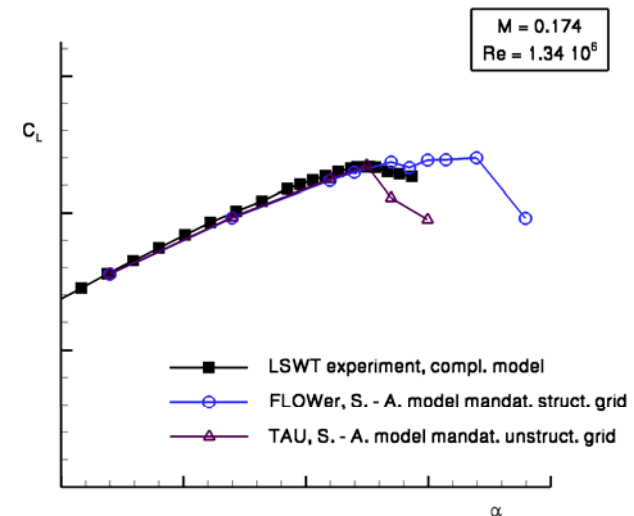
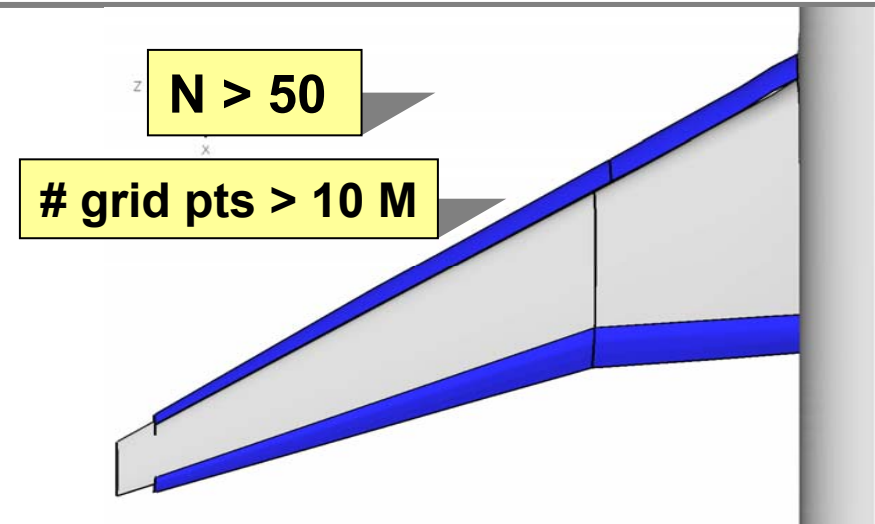


## Problem

- shape optimization in 3D requires large number  $N$  of design parameters
- high computational costs for each flow equations (Navier-Stokes)
- noisy cost functions
- constraints

## Optimization strategies

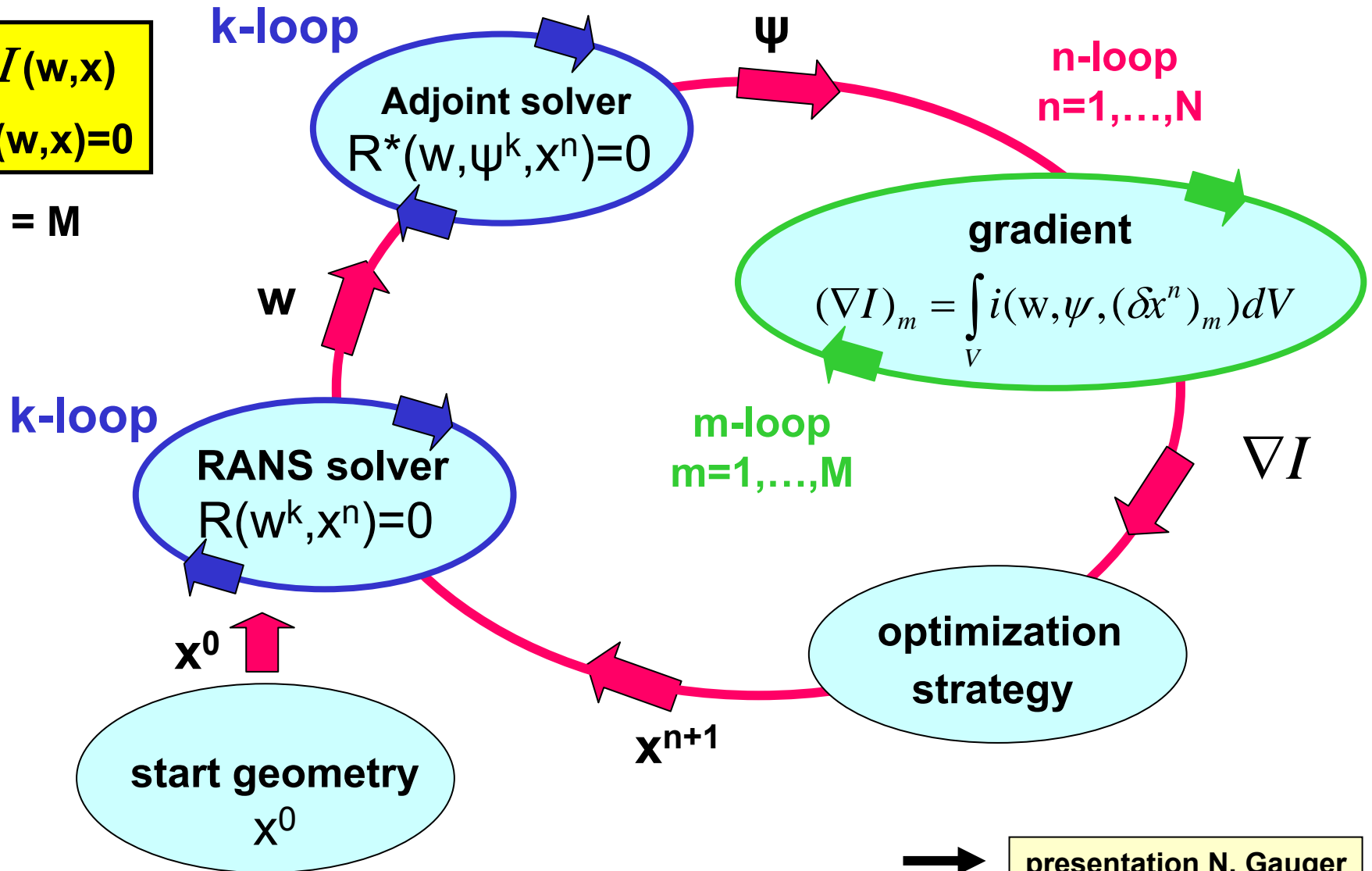
- evolutionary strategies
- deterministic strategies
- gradient based strategies



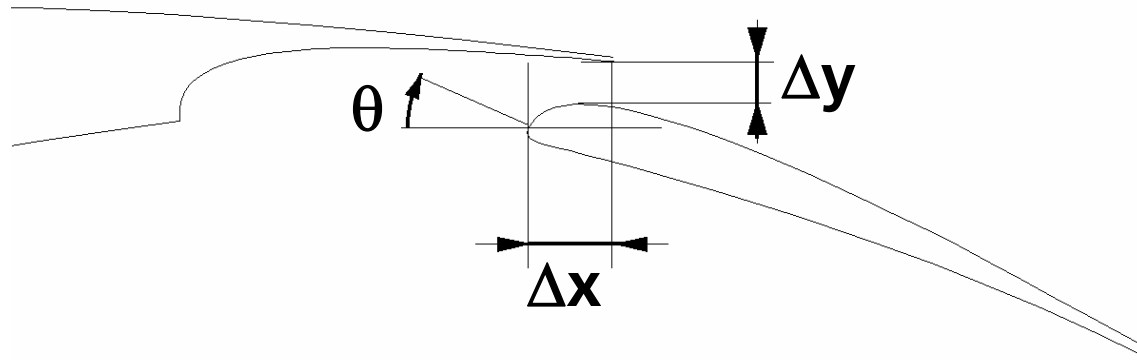
# Adjoint based Optimization

$\min I(w,x)$   
 s.t.  $R(w,x)=0$

$\dim x = M$



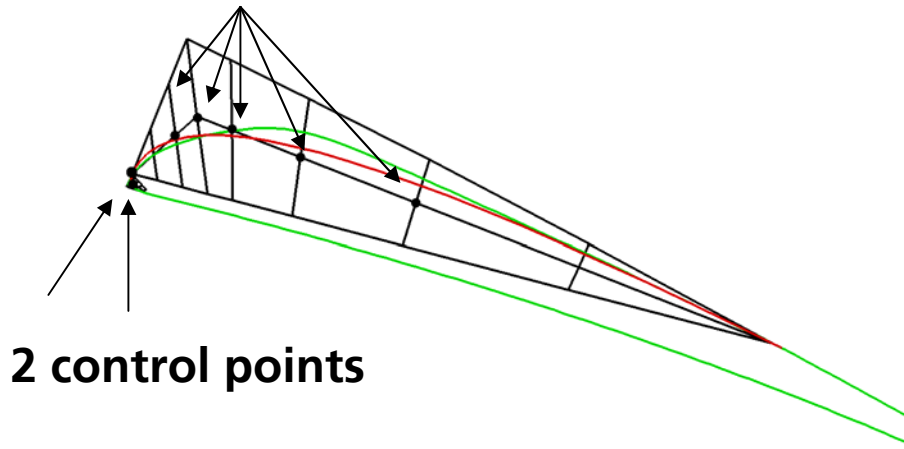
# Parameterisation (10 design parameters)



## Flap position and angle

- ▶ Flap gap ( $\Delta y$ )
- ▶ Flap overlap ( $\Delta x$ )
- ▶ Flap angle ( $\theta$ )

## 5 control points

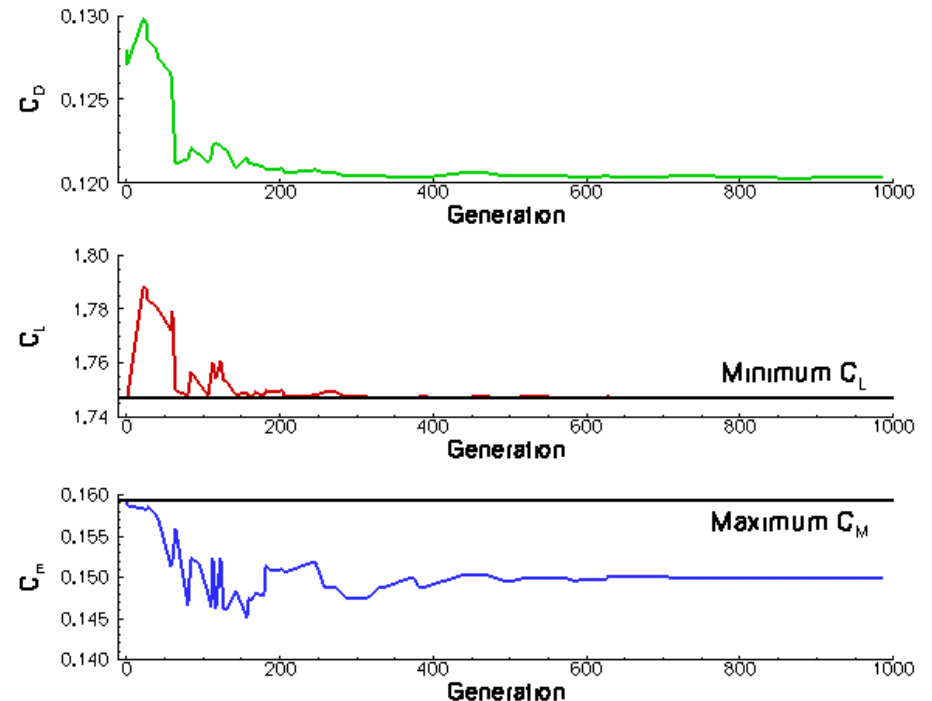
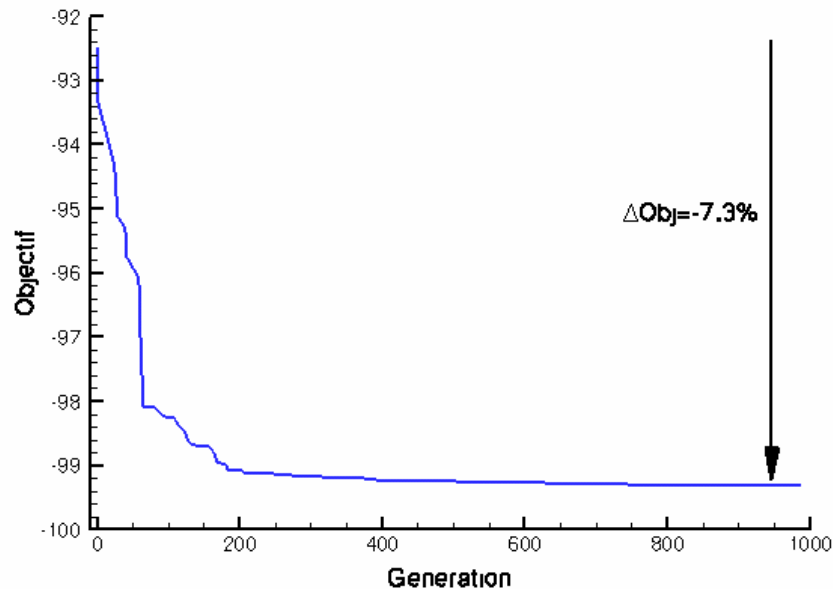


## Shape via Free Form Deformation

- ▶ 5 design at the upper side
- ▶ 1 design at the lower side
- ▶ Nose position

# Differential Evolution (evolutionary algorithm)

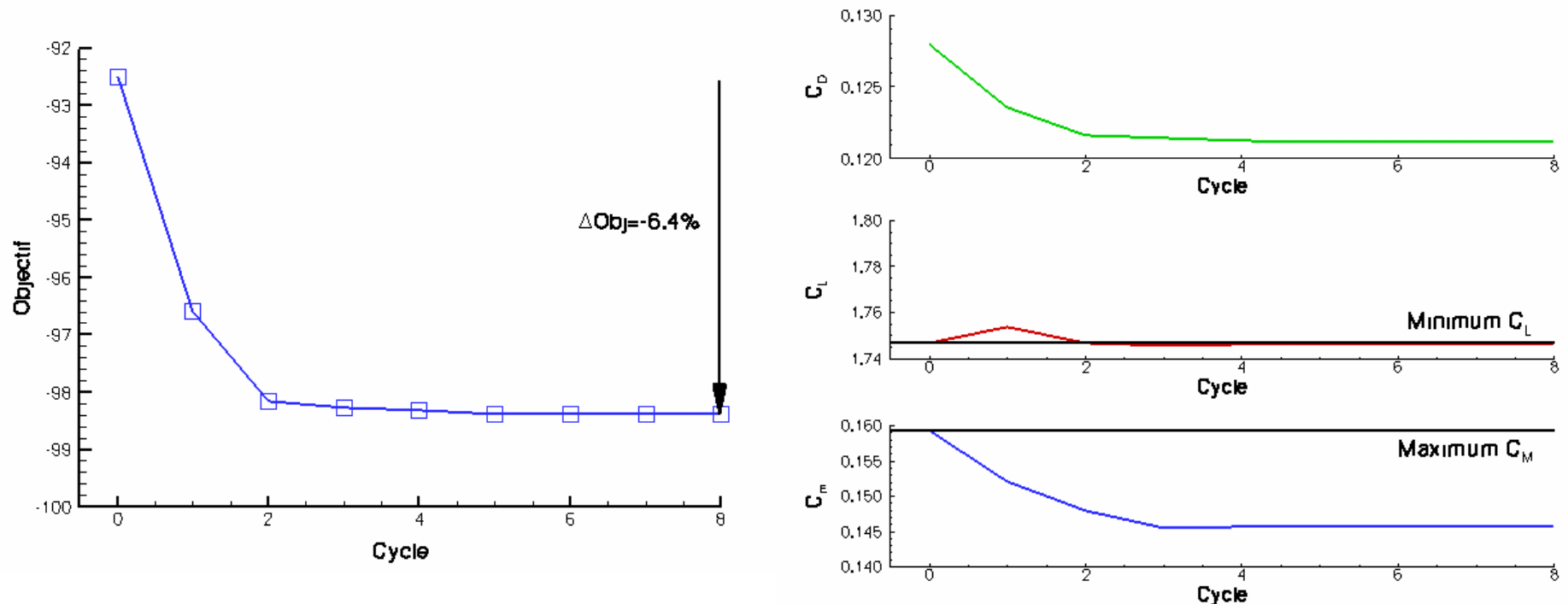
- ▶ 1000 generations, 10 individuals per generation (10.000 evaluations)
- ▶ Best solution after 964 generations ( $\eta=9.649$ )
  - 7.3% improvement
  - $CD=0.940*CD(\text{baseline})$  ;  $CL = CL(\text{baseline})$  ;  $C_m < C_m(\text{baseline})$





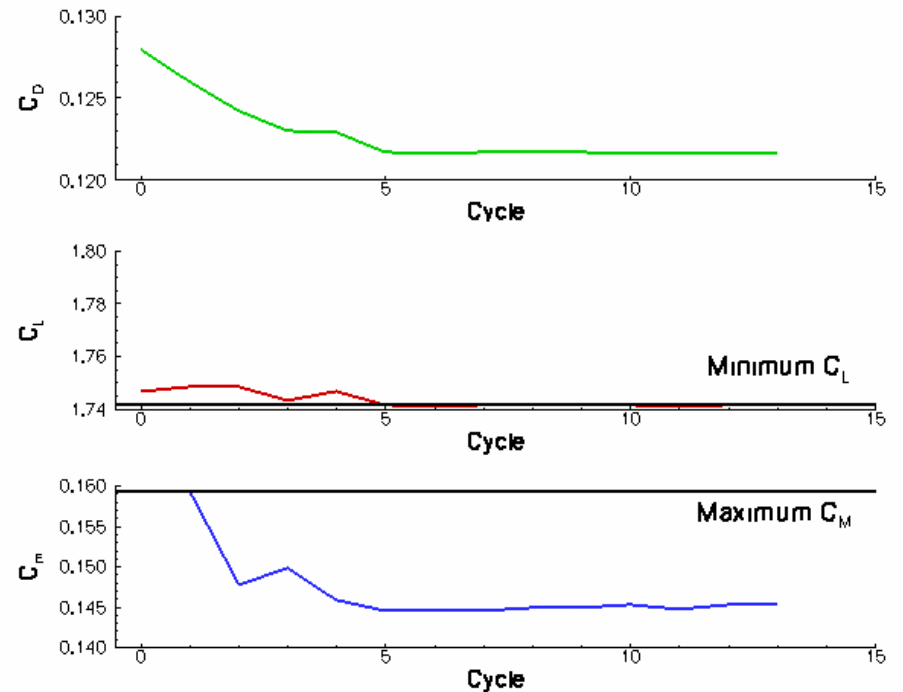
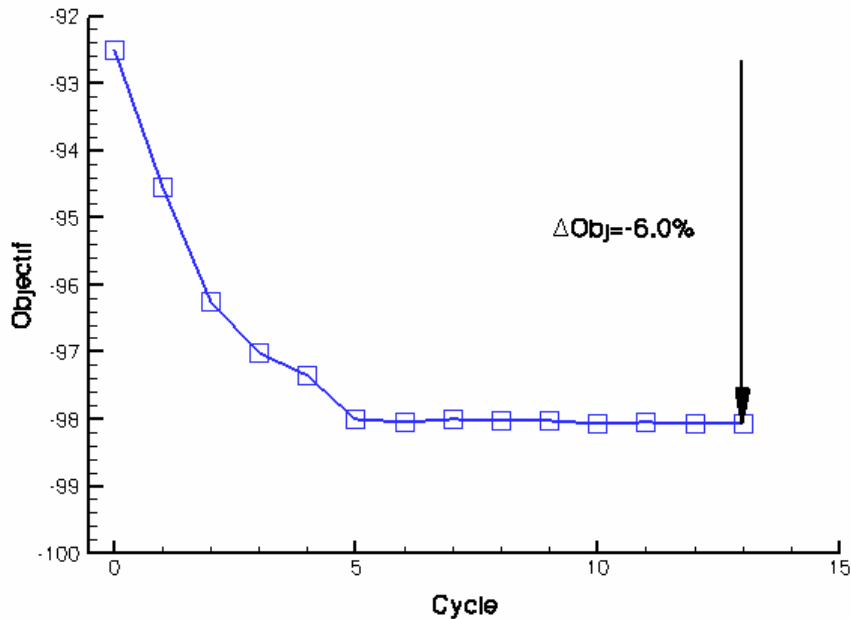
# Simplex (gradient free approach)

- ▶ 8 cycles (549 evaluations)
- ▶ Best solution after 8 cycles ( $\eta=514$ )
  - 6.4% improvement
  - $CD=0.947*CD(\text{baseline})$  ;  $CL = CL(\text{baseline})$  ;  $C_m < C_m(\text{baseline})$

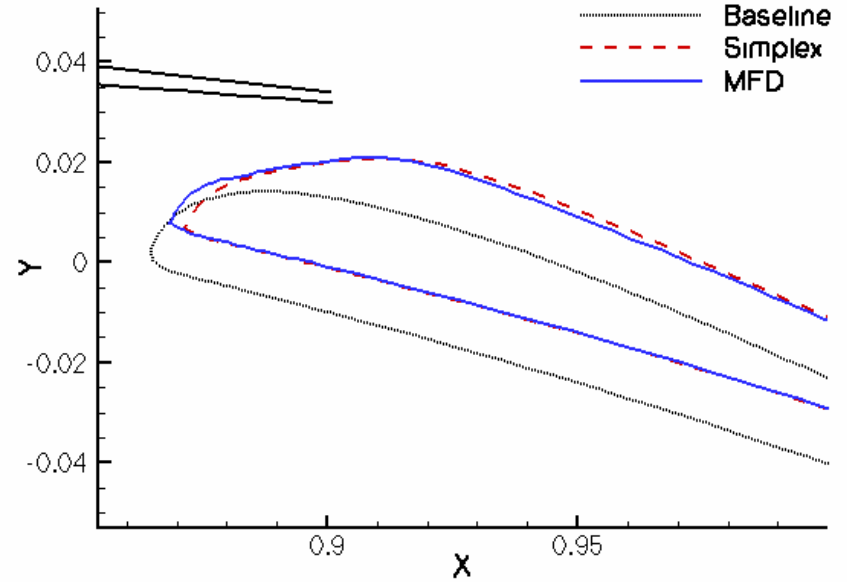
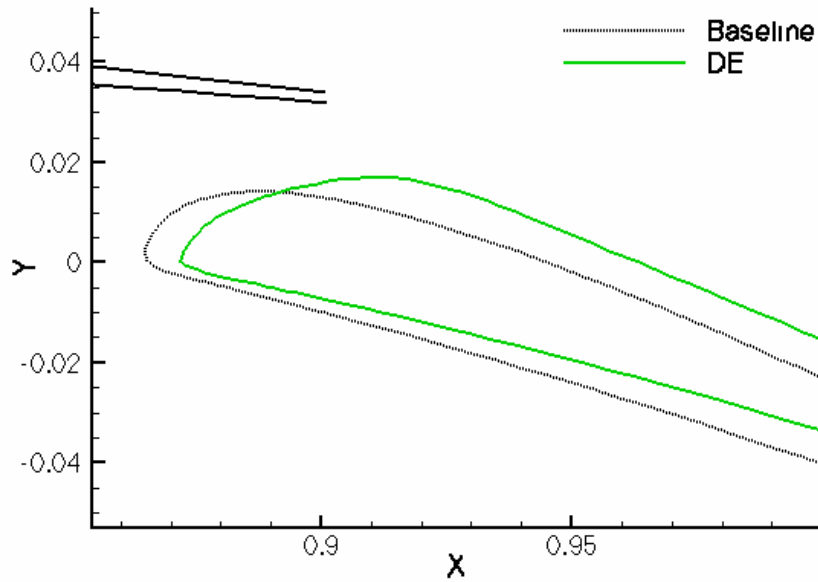


# Method of Feasible Directions (first order approach)

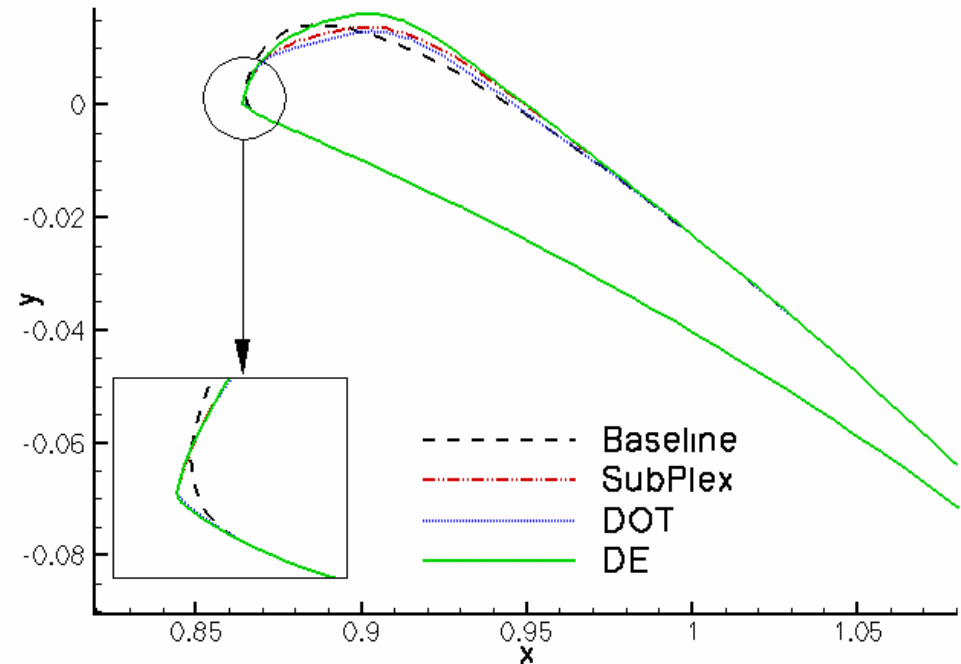
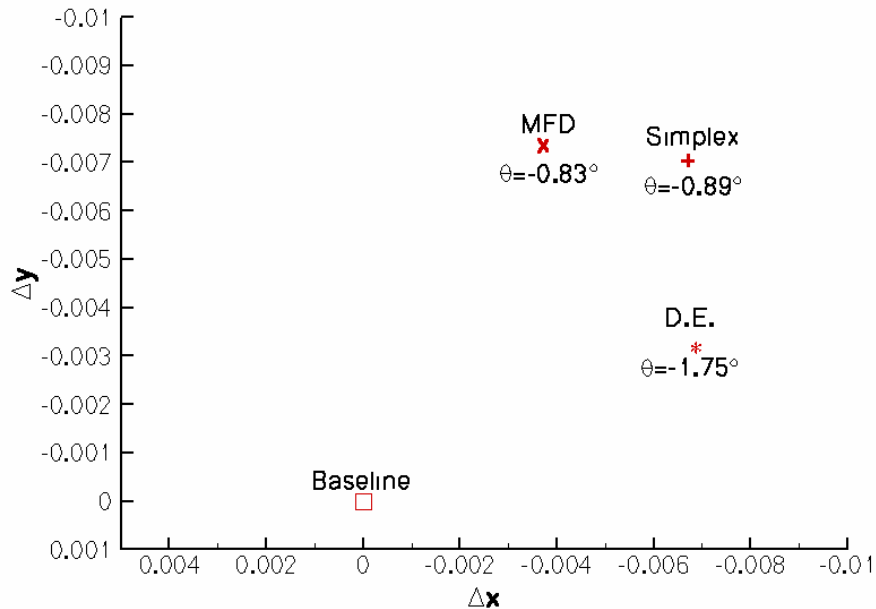
- ▶ 14 cycles (195 evaluations)
- ▶ Best solution after 12 cycles ( $\eta=180$ )
  - 6.0% improvement
  - $CD=0.951 \cdot CD(\text{baseline})$  ;  $CL = 0.997 \cdot CL(\text{baseline})$  ;  $C_m < C_m(\text{baseline})$



- ▶ MFD and Simplex provide close results
- ▶ DE provides an other design



# Flap Design - position and geometry



- ▶ With DE, flap mainly retracted (x direction)
- ▶ MFD and Simplex provide same gap (y direction)
- ▶ MFD and Simplex provide quite same shape
- ▶ Sharp nose obtained in all cases



# Synthesis from the flap design with 10 design variables on the coarse mesh

---

## Differential Evolution

- provide the best optimum
- easy to use, robust, no extra operation from the user
- provide a complete database
- rather long to converge but easily scalable (180 wall clock hours on cluster of 5 computers)

## Simplex

- easy to use and robust to noise
- faster than DE (61 wall clock hours on 1 pc)
- trap to local minimum

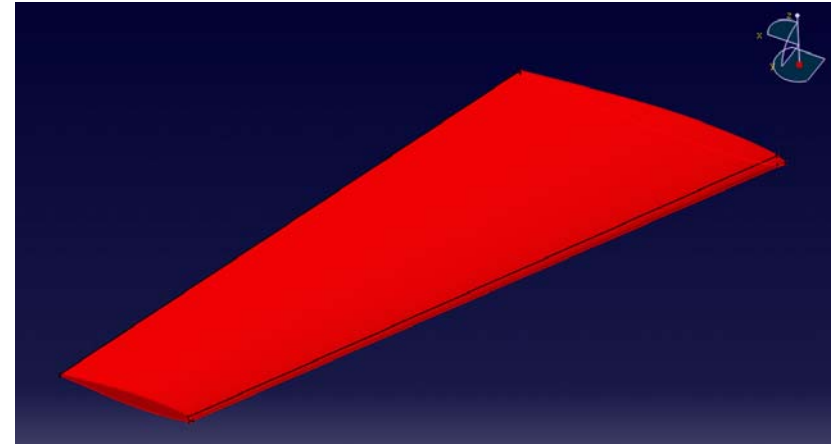
## MFD

- extremely fast (25 wall clock hours on 1 pc)
- lot of "try and error" to get a good optimization (scaling of the design variables)
- not robust (need accurate solution)
- trap to local minimum



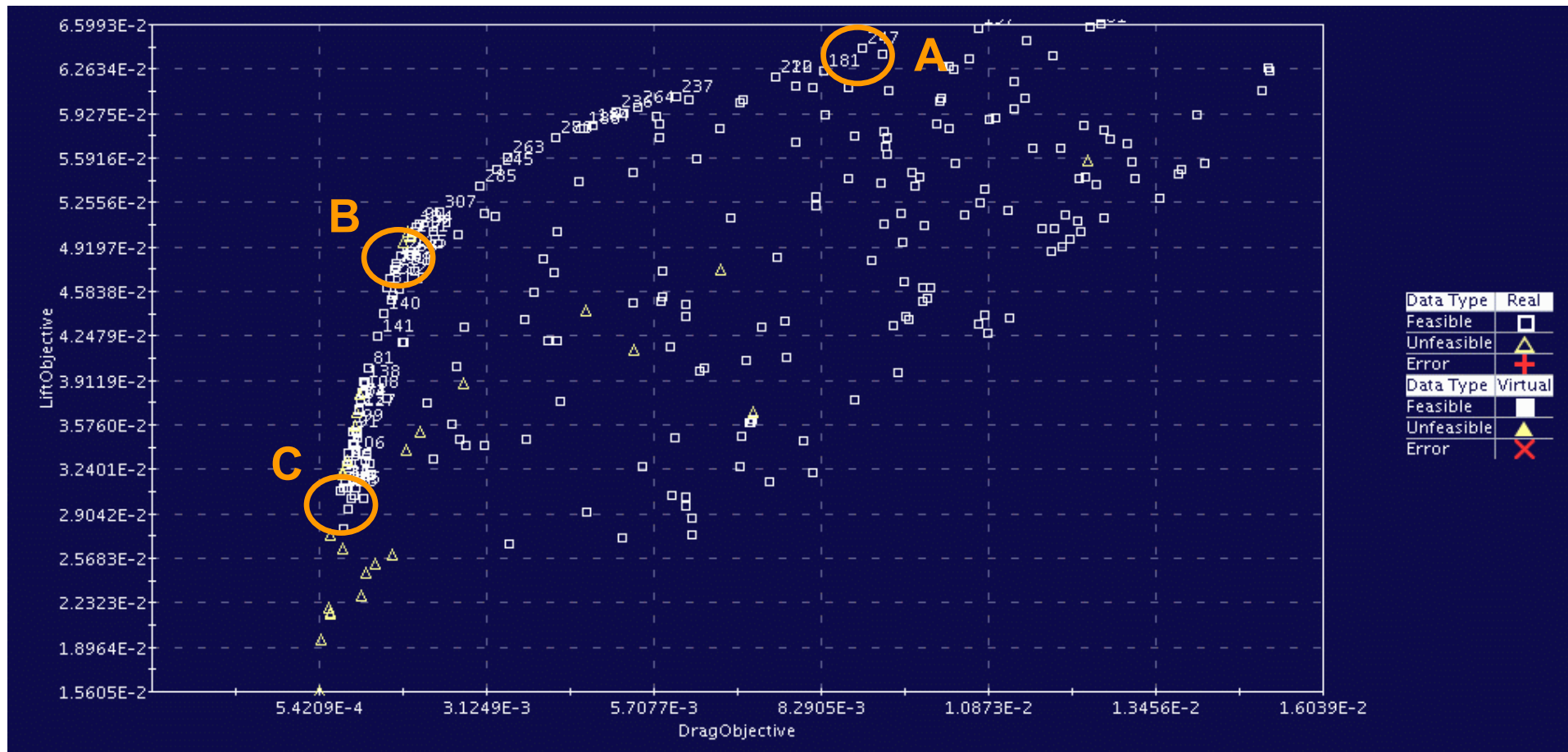
## Shape optimization of wing plan form

- flow condition:  $M = 0.85$ ,  $\alpha = 1^\circ$
- inviscid flow (Euler)
- computational mesh: 630.000 nodes
- **multi objective optimization:**
  - **maximize lift and minimize drag**
- design parameters:
  - sweep angle (range:  $-60^\circ$  to  $+60^\circ$ )
  - half span (range: 0.750 [m] to 1.250 [m])
  - aspect ratio (defined by const. wing plan area constraint)
  - taper ratio (range: 0.2 to 0.8)
- design constraints:
  - pitching moment restricted to range  $-0.025$  to  $+0.0001$



## Wing plan form optimization

Genetic algorithm



Pareto Front

# Multi-Objective Optimization - Example

Flow

**A**

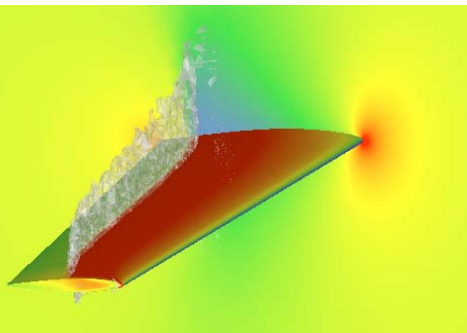
sweep = 20°  
 aspect r. = 6.6  
 taper r. = 0.58  
 half span = 1.250 [m]

**B**

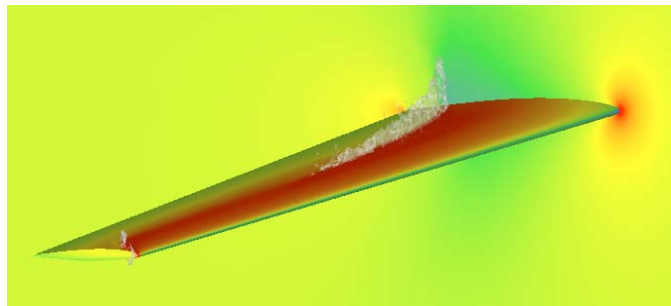
sweep = 36°  
 aspect r. = 6.3  
 taper r. = 0.5  
 half span = 1.250 [m]

**C**

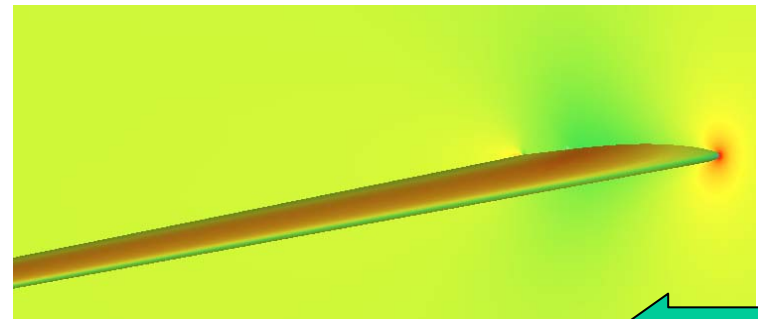
sweep = 50°  
 aspect r. = 6.6  
 taper r. = 0.67  
 half span = 1.215 [m]



lift = 0.064  
 drag = 0.0089  
 moment = - 0.022  
 glide ratio = 7.2



lift = 0.048  
 drag = 0.0018  
 moment = - 0.025  
 glide ratio = 26.7



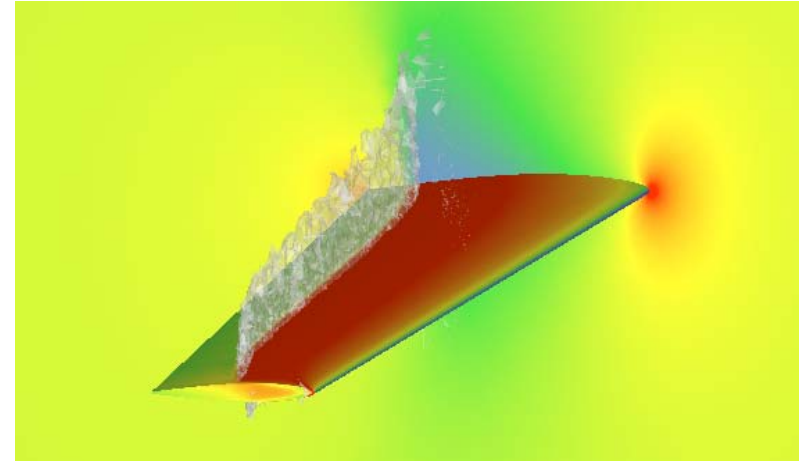
lift = 0.031  
 drag = 0.00087  
 moment = - 0.024  
 glide ratio = 35.6

Flow

## Shape optimization of wing plan form

### Computational effort:

- for one design evaluation:  
50 min (4 XEON 2.6 GHz processors)
    - complete mesh generation time: approx. 15 min.
    - complete flow simulation time: 35 min.
  - 12 concurrent design evaluations using 4 processors each
  - 30 design generations
  - **all together 360 design evaluations in less than 25 h**
- but just 5 design variables and inviscid flow !**



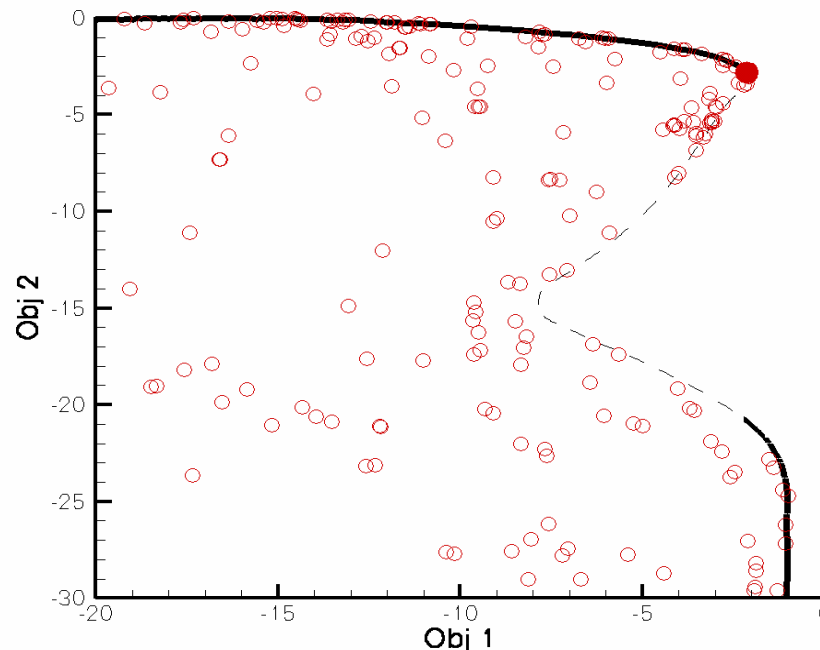
alternative strategies ?

## Academic test case: 2 objectives

### Multi-objective optimisation using Genetic Algorithm

- ▶ Latin Square DOE
- ▶ Population size of 64 individuals  
(i.e. 64 concurrent evaluations could be performed in parallel)
- ▶ 6 generations
- ▶ 383 evaluations

Almost the complete  
Pareto front is captured  
within a single run !

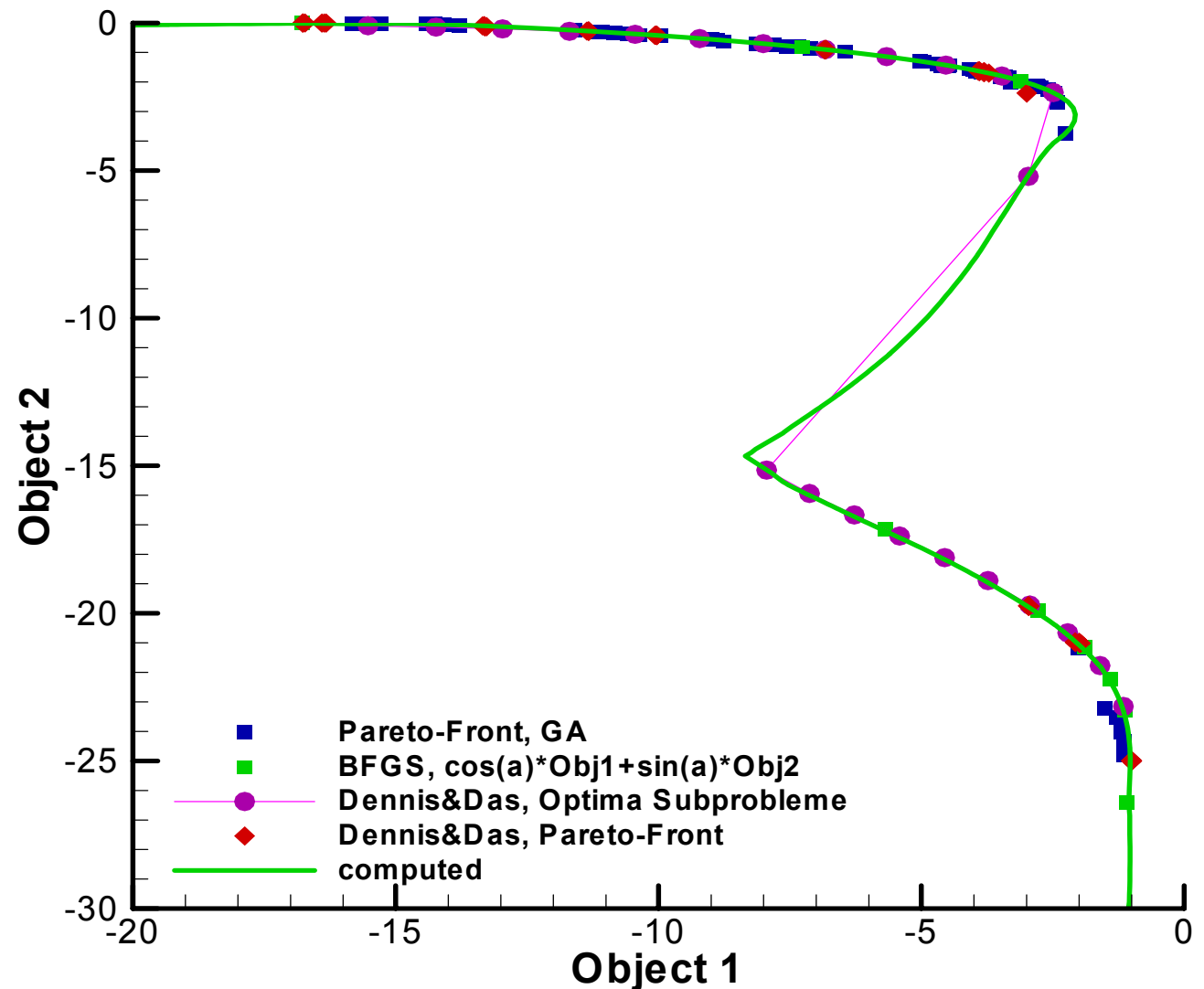




Academic test case

Method of Dennis & Das

Pareto front is calculated through set of nonlinear constraint problems



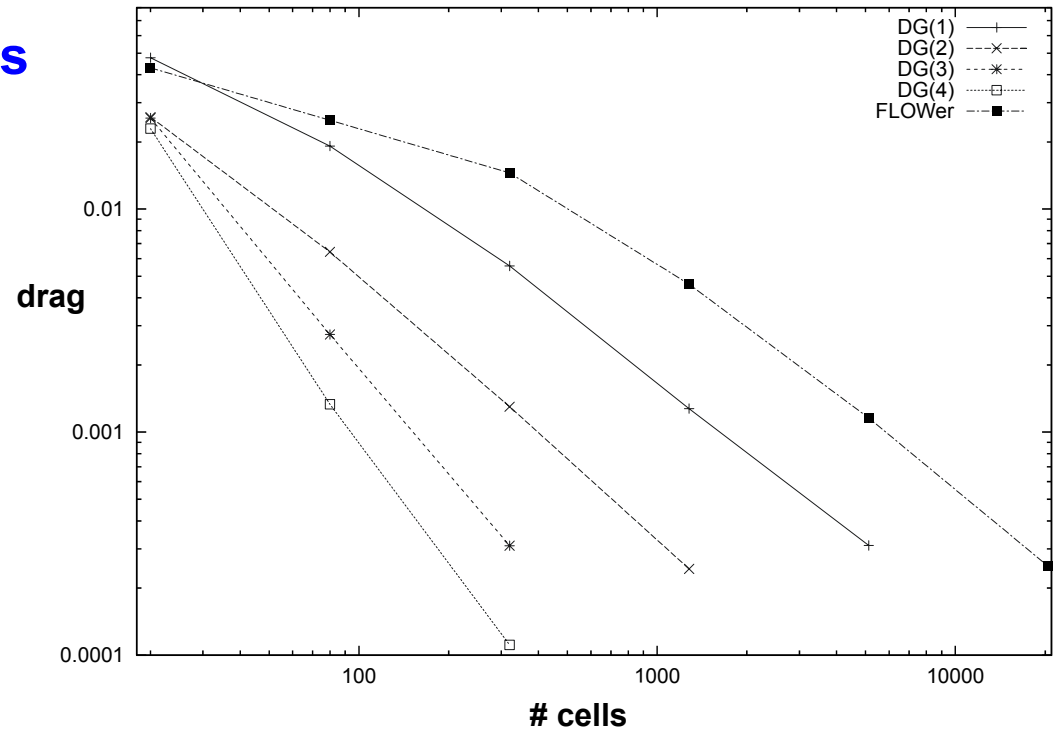
- **CFD mature tool for aerodynamic analysis of complex aircraft configurations**
- **aerodynamic optimization based on high fidelity CFD not yet fully exploited**
  - **large scale applications**
  - **lack of efficient and reliable optimization strategies**
  - **lack of suitable algorithms for geometric modeling**
  - **....**
- **new innovative CFD algorithms and optimization strategies required**
- **focus on multi-objective optimization**

## Discontinuous Galerkin methods

- higher order methods
- (h,p) refinement

### Example

- NACA0012, subsonic
- inviscid computation



grid convergence

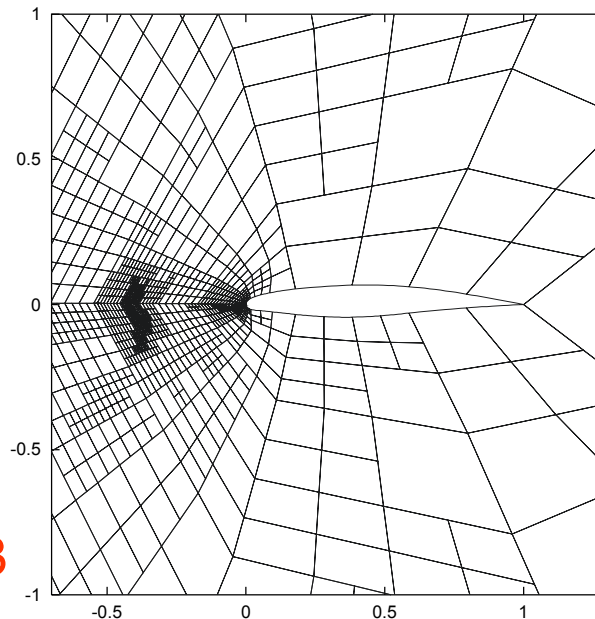
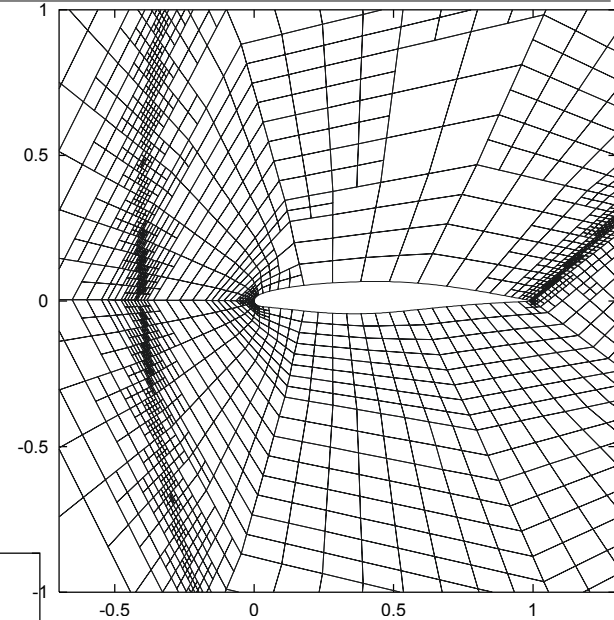
## Innovative grid adaptation

- goal-oriented
- dual-weighted residual indicators (adjoint solution)

## Example

- BAC3-11 airfoil
- $M = 1.2, \alpha = 5^\circ$
- **target:**  
find pressure at leading edge to best accuracy  
 $J(u) = p(x_l)$
- Reference value:  $J(u)=2.393$

residual indicator  
13719 cells  
 $J(u) - J(u_h) = 0.035$



dual-weighted residual indicator  
1803 cells  
 $J(u) - J(u_h) = 0.003$