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Adaptive Discretisation of Shell Problems

A seven parameter Rei β ner-Mindlin shell kinematic is employed for a elastoplastic material with hardening. The resulting nonlinear minimization problem is discretised within a finite element method on the mid surface of the shell. A posteriori error estimates are discussed and related adaptive algorithms are presented. Numerical examples illustrate the theoretical results.

1. Model Problem

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The model problem investigated is a cylindrical shell with the thickness t. It occupies the domain $S(z, \varphi, r) = \{((1+r)\cos\varphi, -(1+r)\sin\varphi, z)\}, -t/2 < r < t/2, 0 < z < L, 0 < \varphi \leq 2\pi$ and r being the distance from shell mid surface S(r=0). The displacement U^{3D} on S is given in terms of functions on the mid surface. The resulting displacement is used in elastoplasticity for small displacements. The displacement U^{3D} is described by a set of 7 functions, or a 7 parameter kinematics,

$$U^{3D} = (u - r\theta)\mathbf{e}_z + (v - r\phi)\mathbf{e}_{\varphi} + (w - r\psi - r^2\eta)\mathbf{e}_r.$$
(1)

2. Principle of Virtual Work

For an arbitrary material law, the principle of virtual work reads

$$\int_{\mathcal{S}} \sigma : \epsilon(V^{3D}) \, d\mathcal{S} - \int_{\mathcal{S}} f \cdot V^{3D} \, d\mathcal{S} = 0 \quad (V^{3D} \in H^1(\mathcal{S})^3).$$
⁽²⁾

As the testfunctions obey the kinematics, this yields to a strong formulation consisting of seven partial differential equations,

$$\int_{-t/2}^{t/2} \frac{1}{\chi} (f_z + \sigma_{zz,z} + \chi \sigma_{z\varphi,\varphi}) dr = 0, \qquad \int_{-t/2}^{t/2} \frac{1}{\chi} (rf_z - r\sigma_{zz,z} - r\chi \sigma_{z\varphi,\varphi} + \sigma_{zr}) dr = 0,$$

$$\int_{-t/2}^{t/2} \frac{1}{\chi} (f_\varphi + \sigma_{\varphi z,z} + \chi \sigma_{\varphi\varphi,\varphi} + \chi \sigma_{\varphi r}) dr = 0, \qquad \int_{-t/2}^{t/2} \frac{1}{\chi} (rf_\varphi - r\sigma_{\varphi z,z} - r\chi \sigma_{\varphi\varphi,\varphi} + (1 - r\chi)\sigma_{\varphi r}) dr = 0,$$

$$\int_{-t/2}^{t/2} \frac{1}{\chi} (f_r + \sigma_{rz,z} + \chi \sigma_{r\varphi,\varphi} - \chi \sigma_{\varphi\varphi}) dr = 0, \qquad \int_{-t/2}^{t/2} \frac{1}{\chi} (rf_r - r\sigma_{rz,z} - r\chi \sigma_{r\varphi,\varphi} + r\chi \sigma_{\varphi\varphi} + \sigma_{rr}) dr = 0,$$

$$\int_{-t/2}^{t/2} \frac{1}{\chi} (r^2 f_r - 2r\sigma_{rr} + r^2 (\sigma_{rz,z} - \chi \sigma_{\varphi\varphi} + \chi \sigma_{r\varphi,\varphi})) dr = 0.$$

3. A Posteriori Error Indicator

A residual-based a posteriori error estimate can be obtained from the strong formulation above with element contributions η_T and edge contributions η_E . The constants in this reliable a posteriori error estimate depend on the thickness, and efficiency is still open. The local contributions are chosen as error indicator for the adaptive refinement algorithm. Both η_T and η_E are given for arbitrary discrete stresses Σ



4. Numerical Experiments

We discretised the model problem with Q1 finite elements on rectangular grids aligned both to the φ - and z-axis. Due to the adaptive refinement algorithm the discretisation allows hanging nodes. We have done numerical experiments with a point load, a radial load as well as a load tangential to the midsurface. Shown here are one example with point load as well as one example with radial load.



The brightness indicates van Mises stresses $||\text{dev}\Sigma||$. The radial load is given by $f = (z^2 - 1)^4 \cos(2\varphi)\mathbf{e}_r$. It can be seen that for both loads the adaptive refinement algorithm results in finer meshes at areas with high changes in stresses.

Further work will be done in applying the a posteriori error indicator to more general material laws in elastoplasticity and a broader range of finite element discretisations.

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